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**BEAUFORT SEA COASTAL EROSION,
SHORELINE EVOLUTION,
AND SEDIMENT FLUX**

By

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ABSTRACT

A comparison of two editions of 1:50,000-scale NOS charts covering 344 km of coastline provides the basis for a detailed study of coastal erosion occurring over a 30-year period. This study also determines patterns in coastline evolution and their probable causes, and sediment yields from erosion. Excluding the large Colville Delta, advancing on average +0.4 m/yr, the average erosion rate is -2.5 m/yr. Extremes for the long-term average rates range up to -18 m/yr. The coastal plain deposits in one third of the study area are fine-grained mud, with an average erosion rate of -5.4 m/yr. The remaining region is composed of coarser sandy deposits, which erode on average -1.4 m/yr. Thus grain size of bluff material exerts the dominant control on coastal retreat rates. Other important factors include bluff height, ice content and thaw settling, bluff orientation, and degree of exposure to the marine environment. Vertical crustal motion has not played an important role during Holocene time. In calculating sediment yield we treat not only the materials above sea level, but consider that the marine profile to 2m depths is in dynamic equilibrium, and therefore contributes to the sediment yield. The upper part of the eroded section contains up to 75% ice, and the sediment yield is reduced accordingly. The annual yield from coastal retreat thus calculated is $2.5 \times 10^6 \text{m}^3$, with the offshore contribution slightly higher than the onshore contribution. We estimate the annual sediment yield from the adjacent drainage areas is slightly less at $2 \times 10^6 \text{m}^3$.

Studying the recent trends in coastal retreat, and the controlling factors, allows estimating the configuration and location of past and future coastlines. The evolution of coastal embayments and lagoons does not begin with the breaching and coalescence of large lakes, followed by thaw settlement. Rather, the existence of old, coarse-grained, and erosion-resistant barrier island and beach deposits exerts a strong influence on the locus and shape of some of the newly forming embayments, while others remain unexplained.

If the present coastal retreat rates have been sustained since sea level rise stabilized about 5,000 yr BP, then the corresponding ancient shoreline could have ranged from 7 to 27 km seaward of the present one at that time, in accordance mainly with grainsize variations in coastal bluffs. Furthermore, if erosion were operative only to 2-m water depths, as assumed in our sediment yield calculations, 10-20 km wide shallow platforms should be widespread around the Arctic Ocean. Since such platforms do not exist, and since we can show that thaw settling contributes very little to the shape of the marine profile, coastal retreat must be associated with erosion reaching to depths much greater than 2 m. The sediment yield therefore should be manifold larger than we calculated. A growing body of evidence shows that the inner shelf seaward to at least 20-m depth is indeed an eroding surface truncating older strata. Considering the rapid, and deep-reaching erosion, modern deposits found in some of the shallow bays and lagoons cannot serve as sediment sinks to accommodate the materials introduced at the present (Figure 2). The sediment yield from coastal retreat and rivers largely by-passes the shelf. A 2-3 m thick sediment layer draping large regions is a result of ice-keels plowing into underlying strata, mixing these with modern materials and fauna into a transient "roto-till" unit.

Within the conterminous United States, the Gulf of Mexico coast has the highest erosion rates. The Texas coast, in many respects similar to that of the Beaufort Sea, retreats on average ~ 1.2 m/yr, or about half the Beaufort Sea average. Since coastal erosion in arctic regions is restricted to three summer months when waves and coastal currents are active, erosion rates there must be multiplied by a factor of four for a meaningful comparison with the Texas coast, which experiences waves and currents year round. Accordingly arctic erosion rates are 8 times higher than Texas rates. Additionally, arctic fetches commonly are restricted by the ever present polar pack, unlike the long and constant Texas fetch allowing generation of larger and more pervasive waves. Classic wave theory therefore can not wholly account for the sediment dynamics of the arctic coastal zone, and we are left with fundamental questions which are important to future coastal development by petroleum industry.

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INTRODUCTION

Two sets of charts published by the U.S. Hydrographic Service and the National Ocean Survey, showing the shorelines for 1950 and for 1980 respectively, are compared in this study of Alaska's north coast between Drew Point and Prudhoe Bay. The mapping was done in accordance with national standards at a scale of 1:50,000, large enough to allow accurate and comprehensive delineation of coastline changes within the 30 year period (see accompanying mapsheet).

Previous studies (Dygas and Burrell, 1976; Lewellen, 1977; Hopkins and Hartz, 1978; Cannon, 1979; Kovacs 1983; and Naidu 1984), using largely spot measurements from aerial photos and maps (for example fig. 4), have documented rapid rates of coastal retreat (figures 2 through 21 are found on the mapsheet numbered sequentially in an easterly direction along the coast). They also have pointed out large regional differences and rapid changes in island configuration and location over various time spans.

The new 30 year comparison entails complete coverage of the coast within the study area (fig. 1) and allows an accurate determination of coastal erosion rate patterns. The coastal erosion rates together with the yield from upland sources are used to estimate the minimum amount of sediment supplied from the study area to the Beaufort Sea. An attempt was also made to interpret trends in coastal evolution in light of what is known about the unique high latitude modern shelf environments. Attempts to extrapolate paleo shorelines from the presently high transgression rates forced consideration of the continental shelf profile, and its evolution through time. These considerations lead to the realization that the arctic marine environment contains elements that are more erosive than its low-latitude counterpart, partly through the abrasive action of sea ice.

REGIONAL SETTING

Physiography and Surficial Deposits

The coastal plain in the study area is a vast, flat, tundra-covered surface with thousands of shallow (1-2 m) thaw lakes (figs. 3, 20). Along the coast this surface is only 2 to 6 m above sealevel, and rises imperceptibly to the south (figs. 5, 17). The tundra surface is underlain by the Quarternary Gubik Formation (Black, 1964) whose marine, alluvial, and glacio-fluvial sediments are mantled by 2-3 m of late Pleistocene and Holocene thaw-lake deposits, consisting mostly of peat and mud (Williams, et al., 1977). Except for an up to 30 cm thick surface layer, the materials underlying the tundra surface are permanently ice bonded. They contain 60 to 70% of ice in the interstices, and in the form of small but pervasive sub-horizontal ice lenses in the upper several meters. In addition, these upper sediments contain 10 to 20% ice in the form of massive ice wedges (fig. 9 and 10) (Sellmann, et al., 1975). Sandy gravel beaches fronting the coastal bluffs generally are about 10 m wide (figs. 8,

11, and 18) and only several tens of cm thick. The active mouths of the Kuparuk and the

Colville Rivers are marked by very low mud flats (figs. 13 and 20), whereas the inactive distributaries are generally marked by 1 m high tundra covered surfaces (fig. 12). About 5 to 8 km from shore an island chain stretches from Harrison Bay to Prudhoe Bay. These are mostly low (1-2 m high) and narrow barriers composed of sand and gravel. Pingok, Bodfish, Bertocini, and Cottle Islands are exceptions in that they contain remnants of the tundra-covered coastal plain with higher elevations corresponding to adjacent land areas (figs. 18 and 20). Harrison Bay and the stretch of coast from Cape Halkett to Drew Point are not protected by islands, with the exception of the sand bar across the large breached lake at Pogik Bay (fig. 3).

The 2-m isobath, which roughly corresponds to the ultimate thickness of the seasonal fast ice, marks a distinct change from a flat inshore bench to a steeper-sloping seaward profile. The outer edge of this so called "2m bench" (Barnes and Reimnitz, 1973) is often slightly shallower than the waters some distance landward. We include this feature on the comparative maps (sheet 1) and in our sediment budget calculations as its outer edge is 1) an important morphologic feature (Reimnitz and Bruder, 1972), 2) the boundary between texturally well sorted sands inshore, and poorly sorted sandy muds offshore (Barnes and Reimnitz, 1973), 3) controls sea ice zonation (Reimnitz, et al., 1978), and 4) is the outer boundary to which seasonal bottom freezing occurs (Reimnitz and Barnes, 1974). In Harrison Bay the 2m bench is up to 10 km wide, elsewhere it is only 0.5 to 5 km wide.

Wave Exposure

The sea surface is completely ice covered for 9 months each year (fig. 3) and even during the short open-water season fetch and waves are minimized by the abundance of drifting ice (figs. 14B and 20). On any usual summer day a skiff can therefore safely land on a seaward-facing beach (fig. 19), while in the lagoons the relatively ice-free conditions lead to greater wave activity. Winds from the northeast dominate, and movement of the littoral drift, coastal currents, and ice drift are to the west (U.S. Department of Commerce, 1981, p.57). Even during rare periods when much of the continental shelf is ice free some grounded ice will usually collect and remain in the nearshore zone.

Shore Processes

Nummedahl (1978) reviewed available littoral transport estimates and concluded that the average transport is westward at a rate of "a few tens of thousands of cubic meters per year". A more thorough evaluation of Beaufort Sea coastal processes by Owens, et al., (1980) quotes a transport rate of 2,000 to 5,000 m³/yr. Reimnitz and Kempema (1983) give similar transport rates for bedload material in a several kilometer wide coastal belt, based on measurements made along the outer part of the 2m bench, several kilometers from shore. This transport again is mainly to the west due to prevailing easterly winds.

The sediment transport is not driven by waves and currents alone. Grounded ice in the nearshore seems to play a more important role in various ways besides its bulldozing action. When worked by storm waves (fig. 16A), this ice acts to intensify turbulence resulting in increased sediment suspension and transport, and a highly irregular "ice-wallow relief" is imparted to the beach and shoreface (Reimnitz and Kempema, 1983) (figs. 7 and 18). This irregular relief in turn when attacked by normal waves results in increased bottom instability, sediment re-suspension, and transport. During open-water storm conditions these combined processes can act in a coastal belt up to 1000 m or more wide, bringing about accelerated bottom erosion and thereby steepening of the foreshore. This in turn can result in accelerated coastal retreat. Under such conditions as much as 30m of coastal plain deposits can be eroded within a period of several days (Short, et al., 1974).

With the coastal deposits being ice-bonded and air and ocean temperatures near the freezing point, factors other than the energy level of the marine environment affect coastal processes. In

this environment unique processes occur. In most cases retreat of the coastal bluffs involves the process of thermo-erosion which includes the following: a) formation of a thermo-erosional niche, when a turbulent sea is brought in contact with bluffs (figs. 9, 10, 11, and 18), b) collapse of bluff materials (figs. 2 and 5), c) slumping, and d) saturated flow of thawed sediments. The mechanisms are described in detail by Harper (1978). A pre-requisite for initiation of these mechanisms is that sea level overtop the protecting beach. Normal summer storms blowing from northeasterly directions result in lower sea levels, exposure of the upper part of the 2m bench with waves breaking some distance from the bluffs. The formation of a thermo-erosional niche therefore is most commonly seen with westerly winds raising sealevel in the Beaufort Sea, and particularly with storm surges (Reimnitz and Maurer, 1979). Storm surges are rare and yet bluff erosion probably contributes the largest amounts of sediment to the sea during these short periods. At these times sediment transport is opposite to the long-term westward movement (Reimnitz and Maurer, 1979). The highest rates of thermo-erosion associated with niche development occur in areas of fine grained, ice rich coastal plain deposits widespread in the western third of the study area. In these areas sparsity of sand and gravel in eroded bluff material does not even permit the formation of beaches (fig. 5).

In the littoral zone and on the beaches along the Canadian arctic and Chukchi Sea coasts, seasonal variations in the depth to the upper surface of ice-bonded sand and gravel have been monitored (for example Harper et al., 1978). The bonded and presumably erosion resistant materials are generally less than a meter below the sediment surface both at the beach and at wading depths near the beach. According to theoretical calculations (Harper, et al., 1978, Taylor, 1980) maximum thaw rates of only 50 to 70 cm/day are indicated for storm conditions when released sediments can be removed at the same rate, thereby maintaining direct seawater contact with ice bonded sediments. Along the Beaufort coast much faster beach retreat rates have been documented. Harper, et al. (1978) speculated that here ice-bonding is not as widespread. However, permafrost studies, for example by Morack and Rogers (1981), and our own probing with rods indicate shallow ice bonding along the Beaufort Sea coast beaches and in the nearshore. Morack and Rogers (1981) demonstrated that the cores of rapidly migrating barrier islands (Reindeer and Cross Island, just east of study area) contain only sporadic bonding. According to jet drilling on these islands, the non-bonded materials seem to be brine pockets (Osterkamp, oral communication, 1985). Such sporadic ice-bonding suggests that the shoreline configuration of these islands during storm erosion should show irregularities corresponding with patchy ice bonding. We have weathered numerous storms behind these islands in our small vessels, and walked the islands without noting such irregularities in beach configuration. Theory, and measurements made elsewhere, therefore do not agree with our observations which suggest that ice bonding of beaches does not retard the transgression rate of the Beaufort Sea across the coastal plain.

The onset of winter, with decreasing water temperature, brings about conditions that have received very little study. In many polar regions the formation of an ice foot (Owens, 1982) is an important phenomenon. There are many forms and types of ice foot (Dionne, 1973), and a treatment here is not necessary. Once formed, an ice foot armors the beach, arrests erosion, and in many cases even results in beach accretion. The fact that sediment layers are interbedded with ice during the growth of the ice foot implies sediment movement from the foreshore onto the beach, and consequent steepening of the shoreface. In rare instances an ice foot does form along the Alaskan Beaufort Sea coast (Short, et al., 1974). However, our observations over many years during the fall, winter, and spring storms in the Beaufort Sea, with and without adequate fetch for wave generation, lead us to believe that ice foot is of little consequential to Beaufort Sea coastal processes. Stratified sediments on the beach face are ice bonded during cold storms, but erosion proceeds rapidly by ripping slabs of bonded sand and gravel from the beach (fig. 14C) and moving these in the swash zone, still intact, for some distance along the beach. During such times the back of the active beach generally is defined by a 1 to 1.5 m high vertical cliff of ice bonded sand and gravel (fig. 14C).

Littoral processes previously not documented for polar seas are those related to the formation of underwater ice (Martin, 1981) in the surf zone. Anchor ice, one form of underwater ice, is produced when water is so agitated at subfreezing temperatures that an ice cover can not form. The water becomes slightly supercooled and ice nucleates on the bed. This process is well documented in high latitude environments such as fresh water streams (Arden and Wigle, 1972, Tsang 1982, Osterkamp 1978). Our own observations, made during three different fall storms with 25 knot winds and air temperatures of -10°C , indicate that in marine waters less than 2 m deep the sediment becomes ice bonded. In one instance a 150 m diving traverse from the beach to 5 m water depth (Reindeer Island, October 1982) revealed ice-bonded sand and gravel interbedded with ice layers in a 30 m wide zone near shore. From the 2-m isobath seaward the seafloor was not ice-bonded but instead covered with pillow-size masses of ice (fig. 8). These ice-pillows consisted of an outer (10 cm thick) rind of fragile ice platelets, but were massive and sediment laden internally. These observations were made immediately after a three day storm and the bottom may well have been completely ice covered during the peak of the storm. The effects of this ice bonding and anchor ice formation on the coastal processes during fall storms is a matter of speculation. Our sketchy observations serve to demonstrate how little is actually known about arctic nearshore processes during times of severe fall weather; yet it is during this period that the greatest coastal changes occur.

A final littoral process to consider is the action of bulldozing of materials by ice from the littoral zone onto seaward facing beaches and barrier islands (Barnes, 1982; Kovacs, 1983). This process occurs mainly on those stretches of coast facing the open ocean and rarely in protected lagoons. The resulting ice piles normally contain sand and gravel that is left as hummocks after the ice melts (fig. 15). The processes were extremely active during the winter of 1982/83 based on a decade of observations in the study area. The chain of islands from Thetis through Cottle Island was marked by sand and gravel piles with average estimated volumes of at least a cubic meter per meter of shoreline. In one area a comparison of composition and distribution of the material shoved onto the beach by ice, and that of the nearshore sediment showed that the bulldozed material originated in large part from the shoreface out to 40 m seaward of the beach. While ice bulldozing during some years may help restore to the shoreface a part of what is lost by waves, currents, and other processes, we feel however, that its overall contribution is small.

METHODS

Retreat rates were obtained for the roughly 344 km of coastline by comparing two sets of charts at a scale of 1:50,000 covering the north coast of Alaska between Drew Pt. and Prudhoe Bay. This comparison is based on the shoreline, registered at mean lower low water by NOS. Some previous studies of coastal erosion focused on bluff retreat, which over short time periods is not always the same as shoreline retreat. For this reason our numbers locally differ from previously published ones, but overall show the same pattern.

The study area was divided into three major segments in order to present the overall coastline on the mapsheet at the desired resolution. Figure 21 serves as a key to these three major coastal segments and the 15 subdivisions used in our calculations. The original C&GS charts (numbers 9466 through 9472) represent the coastline configuration in 1949. The new H.O. charts depict the coastline as mapped by the state of Alaska in 1980. The seaward extent of the eroding coastal zone considered in our calculations is the 2-m isobath. Since the bathymetry was not resurveyed but stems from the original 1949-52 charts, we simply shifted the position of the 2-m isobath (mapsheet) landward in tandem with the local bluff retreat. Bathymetry from the previously undefined small shallow basin, near the coast off sector 9, was delineated by our own surveys in 1980, and is the only exception.

A few small areas not covered by the above charts were interpreted by comparing the 1949 coastline on U.S.G.S. topographic maps with the 1980 data. The maps were brought to a common

scale and projection, and changes in the coastal configuration registered using the same methods applied elsewhere. Areas treated in this manner (southern part of sector 6, western and eastern borders of sectors 11, and central part of sector 14) are identified on the mapsheet.

For convenience of discussion, the coast is divided into 15 sectors based on morphologic and geologic similarities. To calculate sediment input from coastal erosion, each of these sectors is in turn divided into 500m long segments numbered from west to east along the coast. The segments are treated individually.

Generalized nearshore geometry

Quantitative estimates of the sediment introduced by coastal erosion are based on the application of a generalized nearshore geometry (fig. 22) for each 500 m segment. In this model geometry, segment length, bluff height, changes in shoreline position, and distance to the 2-m isobath are measured values; whereas the width, slope, and thickness of the offshore component, and the indicated secondary prism dimensions are calculated values. The general model geometry distinguishes between the two different sources of sediment released to the sea during coastal retreat: 1) The sediment contained in the bluffs between the 1949 and 1980 coastal outlines, and 2) the volume eroded offshore between the new and old nearshore profiles out to the 2-m isobath. For a few particular segments (~ 14% of those studied) alternative geometries were applied. These are described under "Special case geometries" (fig 24.). Tabulated in the Appendix are all measured and calculated values, and parameters assumed in determining the sediment contribution from each of the 500m segments comprising the 15 sectors.

Sediment yield from bluff erosion

To calculate the sediment contribution from bluff erosion we use the 30 year coastal retreat distance (assuming bluff and shoreline retreat in tandem), bluff height, and the ice content of the eroded material (figs. 22, 23). Because the topographic elevations presented on published maps generally are several meters too high (Lewellen, 1977) the bluff height used in our calculations are obtained from the field notes of D.M. Hopkins, and S. Rawlinson, Reimnitz, and Barnes. In determining percentage of excess ice for the coastal plain sediments we referred to a data compilation by Sellmann, et al., (1975), giving excess ice content versus depth below the tundra surface for coastal plain deposits of the Gubik Formation near Barrow, Alaska (fig. 23). The eroded bluff materials in sectors 7 through 15 are coarser grained than those near Barrow, and therefore our assumed ice percentages here are somewhat high. However, in the rapidly eroding sectors 1 through 6 the coastal plain deposits are very similar in lithology, and therefore presumably ice content, to those at Barrow. Sellmann, et al., (1975) assume an in situ after-thaw-settlement porosity of 35 to 40%, while we assume that marine dispersal of sediment results in deposits of only 30% porosity.

In progradational or accreting areas of the coast, we calculated volumes for above sealevel material assuming elevations of 20 cm and 40 cm for delta mud flats, and beaches and spits, respectively. The use of these particular values is based upon our estimates from field observations.

Sediment yield from offshore erosion

To calculate sediment contributions to the sea from the erosion of seafloor material between the shoreline and the 2-m isobath we assume that the slope of the seafloor in this area of the nearshore is in dynamic equilibrium and remains constant as the shoreline retreats. This assumption is based on our local marine surveying experience. The distance of a vessel from the coast and the corresponding water depths, at almost any location, match those on 30 year old published nautical charts. This coincidence, and serious questions concerning the maintenance of such an "equilibrium profile" are discussed in detail later using a site in the western portion of the study

area as an example.

Figure 21 shows schematically the geometry of the eroded offshore areas and how we normally calculated the resulting sediment volumes. We assume no excess ice for the reworked offshore layer, which generally is only 10 to 20 cm thick (see sector tabulations 1-15 in Appendix). Assigning excess ice percentages according to the graph in figure 23 for the submerged layer changes our total volume estimates by at most 10%.

Where the 2-m isobath is highly crenulated, we arbitrarily smoothed it for our measurements. In the previously uncharted area off sector 9, where published charts place the 2-m isobath at 11 to 14 km from shore, we attempt to reduce possible errors by introducing bathymetry delineated from our own surveys in 1980.

Special case geometries

There are several exceptions to the general approach outlined above. The primary differences lie in deviations from the idealized geometry to more closely approximate volumes for unique local configurations. In all of these instances the special case geometries applied are identified and keyed to the particular segments concerned (sector tabulations in Appendix and figure 24A-D).

In sector 14 (Simpson Lagoon), where maximum water depths are less than 2m, the offshore volume considered takes the form of a triangular prism of lagoon-floor material whose apex is at the deepest central point of the lagoon (fig. 24A). The geometry applied here assumes that as the coastline retreats, there is no corresponding shift of the offshore margin, and its depth remains constant.

Two of the remaining three exceptions to the general geometry depict settings in which the landward shift of a relatively steep nearshore profile results in the removal of a substantially thicker prism of offshore material. In one case (fig. 24B) the distance covered by the retreating coastline is greater than the distance measured from the shore to the position of the 2-m isobath. This situation is common in the Cape Halkett area (sectors 5 and 6). We believe that using the general model here might result in values that are excessive relative to our generally conservative estimates for the offshore sediment yield. The second such case occurs where onshore migration of a spit or barrier and accompanying shift of the adjacent nearshore profile likewise results in the removal of a very thick offshore prism (fig. 24C). Examples of these type areas are Pitt Point and Pogik Bay. In the Jones - Return Island chain (sector 15) we assumed no volume change for the sand and gravel barrier islands (tan colored) in fig. 20). Even at the large scale used in this study, we were unable to resolve net volume changes in these barrier islands, and treated them as migrational bodies. Their motion is westward, obliquely onshore, or longshore, thereby adding to the overall westward nearshore sediment transport, but not to the overall shelf sediment budget. Similarly for the Eskimo Islands (sector 7), which like the cores of certain members of the Jones islands presently are stationary coastal plain remnants, we were unable to resolve net changes in the overall volume. Here erosion of westerly exposed tundra bluffs appeared to be compensated by accretion on adjacent and leeward beaches and spits.

The last exception to the general model deals with areas of actively accreting or prograding shorelines. Here we assumed a seaward shift of the shoreface and offshore profile, with prograding mud flats and beaches at respective elevations of +20cm and +40cm (fig. 24D). In the overall summary of volumes and weights, the net gain calculated for these areas was subtracted to arrive at the final sediment yield.

RESULTS

For each of the 15 sectors a tabulation appears in the Appendix showing both measured and calculated values used to determine the sediment yield from coastal retreat. These appendices are identified by sector numbers, and are keyed to numbers in figure 21 on the mapsheet. Table 1 summarizes the results for the entire area.

The average rate of coastal retreat for the 344 km of coastline studied is 2.1 m/yr. That rate includes the large Colville River system, with 48 km of coastline advancing an average of 0.4 m/yr. Excluding the delta, the erosion rate is 2.5 m/yr. After subtracting excess ice from the eroded bluffs, we calculate the annual sediment contribution from coastal erosion at $1.2 \times 10^6 \text{ m}^3$. This number is the sum of the sediment yield from all segments divided by 30 years. Using the same approach we calculated the annual sediment contribution from offshore erosion at $1.3 \times 10^6 \text{ m}^3$. The total annual sediment yield from coastal erosion therefore is $2.5 \times 10^6 \text{ m}^3$. To help visualize the significance of this sediment volume one can pro-rate it for the Holocene period (10,000 yrs) and spread it over the present shelf area adjoining the study area ($15,500 \text{ km}^2$). The resulting sediment layer would be 1.6 m thick. As discussed below, however, the offshore erosion associated with the present transgression can not be restricted to coastal waters of less than 2 m deep. The inner and midshelf is a surface of erosion, and the resulting sediment yield may be many times larger than we calculated.

Table 2 lists available sediment textures for coastal plain deposits exposed in bluffs. Christie Point ($155^\circ, 35' \text{W}$) and Tigvariak Island ($147^\circ, 15' \text{W}$) lie outside of the study area. The former is representative of the fine-grained deposits in sectors 1 through 6. The latter was included as an abnormally coarse grained section, as far as we know without counterparts in the study area. Only the data from Rawlinson gives information on the amount of organic matter contained in bluffs. But the 40 % he obtained from his extensive work around Simpson Lagoon probably is roughly representative for the entire region.

DISCUSSION

Regional patterns in erosion rates

There are large regional variations from the 2.1 m/yr average calculated for the 30 year period. Extremes range from an average 30 year retreat rate of 18 m/yr near Cape Halkett, to an average 30 year accretion rate of 20 m/yr near the active mouths of the Colville drainage system (mapsheet). There is a pronounced disparity in erosion rates between the western and eastern parts of the study area. The western portion is entirely composed of fine grained coastal plain deposits extending north from the Pelukian beachline (fig. 26). Retreat rates of bluffs here (sectors 1-6, but exclusive of Pogik bay with its unique setting), average 5.4m/yr. The remaining part of the study area lies east and to the south of the Pelukian beachline where coarser grained materials make up the bluffs. The average retreat rate for this section of coastline, exclusive of the Colville River Delta sector is 1.4 m/yr.

Long term changes in the coastal configuration are dependent on a combination of various climatic and oceanographic factors, as well as on the composition and geometry of the coastal plain transgressed. Severe short-term episodes of coastal erosion may locally play a significant role in the overall evolution of the coastline. An example is the 30 m of bluff retreat on Pingok Island experienced during one season. Most of this retreat occurred during a single storm event of several days duration (Short, 1973). During intervening years bluffs may locally appear entirely stabilized.

An understanding of regional differences in erosion rates in terms of geologic and oceanographic setting, would allow reconstruction of past shorelines, and a prediction of future trends in coastal evolution. Certain factors known to influence the erosion rates will be discussed.

Vertical movement of the earth crust is important in some parts of Alaska for coastal evolution, and will be analyzed first for the study area. The consistent altitude (7 m \pm 3 m) of the Pelukian shoreline from Barrow to the Colville River (Hopkins and Carter, 1980) are strong evidence that that stretch of the coast has been stable for the last 120,000 years. Thus Dease Inlet and Smith Bay, two of northern Alaska's most pronounced embayments, are not the result of differential vertical motion during that time period. According to Hopkins and Hartz (1978) the coastal plain deposits cropping out in the Jones Islands may also be Pelukian beach deposits. If true, the Pelukian beach deposits extend at a uniform level through the entire study area, except for a gap in eastern Harrison Bay. From our seismic records of the region, from industry borehole data, and from onland studies of the Quaternary geology (David Carter, oral communication, 1985), there is no evidence for Holocene subsidence of Harrison Bay.

Mean sealevels for the summer months from 1975 to 1984, measured by the U.S. National Ocean Survey at the east end of sector 14 are shown in figure 25. The best fit line for that data indicates a sealevel rise of 2 cm/yr or 2 m/100yrs. This is much higher than the 0.1 to 0.15 m/100yr worldwide sealevel rise and therefore suggests subsidence of that area. The configuration of shallow subbottom seismic reflectors in the region, in particular that of the Post-Pelukian unconformity offshore, does not support local subsidence. Furthermore, the modern coastal retreat rates in the area of the tide gauge are among the lowest of the entire study area. Thus we can find no support for the 9 yr sealevel trend shown by summer tidal data. All information available to us therefore suggests that irregularities in the coastline of the study area are not produced by differential vertical crustal motion during Holocene time.

Bluff height is one of the dominant factors controlling rates of erosion (Owens, et al., 1980). In areas of high bluffs and accordingly large sediment volumes the marine energy in some cases simply is inadequate to remove material at the same rate at which it is made available by melting. Areas that lack bluffs, as in figure 6, on the other hand are quickly inundated due to the extremely large amounts of ice in the upper 2 m of coastal plain deposits and the resulting thaw collapse. Here little lateral transport of sediment, or 'marine energy', is required to inundate the coastal plain. High bluffs along the Chukchi coast are partly responsible for the much lower erosion rates there than along the Beaufort Sea coast (Harper, 1978). Similarly, high bluffs in the Kogru River area are probably in part responsible for the lower erosion rates there than at Cape Halkett; although in this case the degree and direction of exposure and especially bluff lithology are perhaps the dominant factors.

The presence or absence of a beach, and its volume, strongly affect the coastal retreat process. Broad and high beaches are rarely overtopped by the sea, reducing thermal processes to ineffective atmospheric summer warming. One such area is the north coast of Pingok Island, where for reasons not well understood the beach broadened, even advanced, during the study period, yet the bluff continued to retreat. Because this study compares shorelines, while others may have considered the changes in the bluffline only, our erosion rates may differ from previously published values. The Pingok Island retreat rates shown in figure 32 are from Naidu (1984), and serve as example.

Variation in coastal plain composition (sediment grainsize) is an extremely important parameter. Coastal plain deposits containing pebbles and cobbles in a sandy matrix erode much slower than those composed mostly of silt and clay which have higher ice contents (Hopkins and Hartz, 1978). Areas with fine grained coastal plain deposits are also marked by a lack of protective beaches (fig. 5), due to a scarcity of sand and gravel size particles. The importance of grainsize is evidenced by the dramatic differences in coastal retreat rates between the eastern and western portions of the study area. From Oliktok Point eastward, where the coastal plain is composed of a series of coalescing alluvial and glacial outwash fans extending northward from the Brooks Range (Hopkins and Hartz, 1978); retreat rates are nearly an order of magnitude less than in the area to the northwest between Cape Halkett and Drew Point north of the Pelukian barrier chain (fig. 26) where bluffs are composed of marine mud (Carter and Robinson, 1980). These differences are

partly responsible for the more stable coasts in sectors 12 through 14 (1.3 m/yr) than those of sectors 1 through 6 (5.4 m/yr). The coarse Pelukian beach deposits north of Kogru River (sector 7), and exposed to the east in a number of the Jones Islands in form of high tundra-covered coastal plain remnants (fig. 18, and 20) (Hopkins and Hartz, 1978) are more resistant to erosion and control coastline evolution. Thus, the rapidly retreating promontory between Cape Halkett and Drew Point will likely stabilize at the ancient Pelukian barrier chain on the north shore of Teshekpuk Lake (fig. 26) in a few thousand years.

Degree and direction of exposure to the various climatic and oceanographic processes affect erosion rates. Open water conditions with waves and currents are needed to remove the materials introduced by bluff erosion. Simpson Lagoon is ice free for a greater part of the summer than the "open ocean" waters north of the Jones Islands (see typical ice distribution in fig. 19). The increased fetch in lagoons affords greater potential for erosive processes and consequently retreat rates in the lee of these islands are commonly higher than on the ocean-facing side (sector 15). Water temperature also affects erosion rates, partly owing to more effective niche development, and partly due to the extended open water season near river mouths. The coastal plain remnants in that part of the Jones Islands chain equidistant from the warming effects of the Colville and Kuparuk Rivers may be testimony to this influence. Such old remnants may have long since disappeared in the islands directly off the Kuparuk River, leaving barriers composed only of a thick sand and gravel lag atop residual tundra cores. Cannon (1978) pointed out that southfacing bluffs, those exposed to the sun for the greater part of the day, erode faster than north-facing bluffs. An example of the results of this difference in orientation is partly reflected in the higher erosion rate of bluffs on the south side of Pingok Island. Reimnitz and Maurer (1979) pointed out that storm surges, and therefore westerly winds in general, should be those most effective in producing significantly elevated tide and wave conditions, and thought that for this reason west-facing promontories retreat faster than those facing east. The resulting pattern, as best exemplified by the coastal configuration and retreat rates in sectors 13 and 14, is indicative of processes acting in a direction contrary to those responsible for the westward orientation of the small coastal spits trailing off the mainland promontories. This pattern however does not hold elsewhere in the study area.

Formation of embayments and lagoons by thermal collapse

Wiseman, et al. (1973) showed how thermal collapse of lakes breached by the transgressing sea results in embayments and lagoons (fig. 27). They envisioned a 4 phase evolution beginning with an area of large lakes similar to the Cape Halkett region. The coalescence of such lakes and the breaching and inundation by marine waters to form Kogru River type inlets is their second phase. This is followed by a widening of the inlet, and eventual stranding of coastal plain remnants to form an island-protected lagoon setting similar to that of Simpson Lagoon, as phase 3. The scenario is concluded by citing Leffingwell Lagoon (east of study area) as an example of maturity in phase 4. Reimnitz and Maurer (1979) have pointed out problems with this model, presenting Kogru River and Prudhoe Bay as examples. The lakes in these two regions are currently perched several meters above sealevel. Thus the anticipated amounts of thermal collapse of existing lake beds without subsequent deepening by erosion, could not create the 3 to 4 m water depths found in the two embayments. Also, enlarging the types of lakes found north of Teshekpuk Lake (fig. 26) as in phase two of Wiseman, et al. (1973) would result in water bodies oriented at right angles to the existing major embayments and lagoons we are trying to explain.

The lakes deeper than 2 m in the area north of Teshekpuk can be recognized by their persisting seasonal ice cover in figure 20 (Sellmann, et.al, 1975). Figure 26 indicates actual lake depths according to Holmquist (1978), C. Sloan, USGS (oral communication, 1980) and J.Helmericks, bush pilot (oral communication, 1984). The figure also shows three lakes that have been recently breached by the advancing sea to form very shallow NW-SE oriented embayments. Pogik Bay is one such embayment. The 2-m isobath, perhaps marking the northern part of this former lake basin, juts seaward by about a kilometer from the general trend of that isobath on

either side (see sector 4, Sheet 1). Thus the lake basin is a submerged promontory, more resistant to erosion than the surrounding terrain. Perhaps this can be attributed to the former existence of a deep lake underlain by a thaw bulb lacking excess ice. Upon breaching and inundation such lake bed would be dense and stable, and therefore not subject to further thermal collapse. A similar setting and evolution is described by Tomirdiaro (1975) for a cape in the East Siberian Sea. The cape marks a deep lake basin breached by the transgressing sea. Pogik Bay, however, is generally too shallow for use by even light float planes. The resistance to erosion here may alternatively be due to a thick accumulation of fibrous organic matter on the former lake bed.

The NE coast of present Cape Halkett may mark the west shore of a former large lake breached about 200 years ago. According to Leffingwell (1919, p.170), Dease and Simpson in 1837 mention a passage inside of a tundra-covered island which they named as the original Cape Halkett. Some 19th century charts (for example H.O. Chart no. 68, 1893 edition) show this island elongated parallel to the regional trend of lake axes. On figure 28 we stippled the outline of this island. The last tundra remnants of the island disappeared by about 1945, and in 1952 it was charted as a shoal (sheet 7991). The water depth over the former lake between the cape and the shoal is now less than 2 m.

Thermal collapse resulting in the development of coastal sediment sinks

According to our tabulations the sediment contribution from erosion in the offshore is slightly larger than that from the onshore. But the absolute reliability of the calculated values for this contribution is questionable due to the possibility of thermal collapse in the offshore zone. Harper (1978) in fact stated that "thaw subsidence causes a continual steepening of the offshore profile and provides a sediment sink for eroded sediments." In the following section we will analyze the Russian studies from the Laptev and East Siberian Seas commonly referred to in western literature (e.g. National Research Council, Marine Board, 1982) and then an example profile from our study area for evidence on thermal collapse.

Example from the East Siberian Sea

Russian workers have attributed the most important role in the shaping of the arctic continental shelf profile to thermal processes. Thus Tomirdiaro (1975) states "The eastern Arctic seas are largely young Holocene bodies of water formed by thermo-abrasional processes; it is thermo-abrasion, and not the usual abrasion processes, that has formed the so-called Arctic continental-oceanic zone here in such a short time." His interpretation relies heavily on the marine studies reported on by Klyuyev (1965). The data Klyuyev presents are hydrographic surveys repeated over time intervals of 15 to 20 years, off coasts that are retreating as fast as the coast in sectors 1 through 8 in our study. One of these surveys repeated after 15 years (Fig. 28) suggests a maximum lowering of the seafloor by 0.6 to 0.7 m in the depth range from 2 to 4 m, or a shoreward shift of the 2, 4, and 6 m isobaths by 0.5 to 1.2 km. The seafloor lowering was least adjacent to the coast, and on the outer end of the profile at 6 to 7 m depth. Klyuyev claims that the possibility of errors in navigation or in sealevel datum were definitely excluded in these surveys. We note that the 0-m isobath, which should represent the shoreline, remained stationary while the bluff had retreated by 170 m.

Klyuyev (1965) apparently attributes the depth changes entirely to thermal collapse, and presents evidence that the upper surface of the ice bonded section is at or immediately below the seafloor. The evidence he presents also can be interpreted differently. He reports that short cores may contain several millimeter long ice crystals. We have observed that small ice crystals form in fine grained sediments during fall storms, triggered by a rise in water salinity and a drop in water temperature to slightly below its freezing point. The sediment interstitial water still retains a slightly lower salinity acquired from summer river flow. The ice platelets seem to decay within a month into winter. He also reports ice in sediments and bonded sediments normally submerged areas exposed during strong winds. Ice bonded sediments in the Alaskan Arctic are also near the

surface on the 2m bench, where the fast ice rests on the bottom at winter's end. The thickness of the unbonded sediment layer in shallows, however, is not an indicator of the thickness of unbonded sediments offshore. He further cites as indirect confirmation of the existence of permafrost on the seafloor the following fact: "Vessels drift during a storm even with two anchors. The anchors slip over the solid bottom, and when the depth is slight a characteristic knocking can be heard." The bottom is not rocky where these observations were made. Such observations have also been made during fall storms in the Alaskan Arctic (Jim Adams, tug boat operator, oral communication, 1984). Our own work has shown that shallow water sand and coarser deposits during freeze-up storms become ice bonded and form anchor ice, as discussed earlier. Ice bonding, however, apparently forms only a surface crust, which disappears after the ocean has a new ice canopy. The annual formation of a seafloor crust can not result in net thermal collapse. The principal evidence for submarine thermal settlement brought forth by Klyuyev is the presence in the Laptev and East Siberian Seas of wedge-shaped depressions with peaked flanking ridges, which he interprets to be thermokarst features, resulting mainly from the melting of ice wedges. These are subdued in shallow waters, become best defined with increasing water depth (15 to 20 m), and are found seaward to 50 m water depth. This distribution pattern, with better preservation at increased water depth where sediments are more cohesive than on the inner shelf, and also the shapes of the features in fathograms, match exactly those of ice gouges on the Beaufort Sea shelf (Reimnitz and Barnes, 1974; Barnes, et al., 1984). The features are much too large (120 m wide) to be produced from the melting of ice wedges (* There is a large discrepancy between the 8 and even 12 m depression depth he quotes, and the maximum 5 m we measure from his figures). Lastly we note that thaw settlement in the coastal zone should result in the trapping of most sediments introduced. There should be little chance for sediment sorting, and underlying ice-bonded materials become buried by sedimentary accumulations. Yet the local bluffs introduce silt and clay-size materials, while offshore deposits are sandy. To us this indicates that mechanical, rather than pure thermal energy is at work winnowing the sediments introduced, that steep-sided depressions with flanking ridges are short-lived, and that the sedimentary environment is not unlike that of the Beaufort Sea.

Analysis of a North Slope profile

The following is an analysis of a coastal plain/continental shelf profile in the most dynamic region near Cape Halkett, to shed light on this question of offshore thermal collapse. Figure 29 is the overall profile compiled from published topographic maps and charts. A line on figure 26 indicates the precise location and trend of the profile. This particular line was chosen as an onshore continuation of an offshore profile which we have re-surveyed repeatedly for monitoring the rate of ice gouging from 1977 through 1980.

The coastal plain from the beach for a distance of 35 km inland has slightly undulating relief ranging between 5 and 12 meters above sea level. The last 5 km to the beach are marked by generally decreasing elevations, with a general slope that matches that of the seafloor for a few kilometers onto the continental shelf. The coastal zone is a pronounced niche in this profile, as amplified in figures 29B, 30A and B, and 31.

Unfavorable geometry of the shore stations with respect to the inshore end of the survey line (fig. 26) introduces possible north-south position errors of plus or minus 23 m between our own surveys. The western shore station is located at the corner of the hut at Esook (fig. 5), which has not been surveyed accurately. Thus there is an additional unknown error that affects the comparison between the 1950 and 1980 profiles. Our fathograms show slight local depth differences from one season to another during the 1977 to 1980 interval. But in view of the possible position errors, the overall bottom profiles are similar enough to be shown as a single solid line in figure 29B. This line is relative to a sealevel average for all survey periods, and has a likely error of 20 cm relative to the true datum. Our surveys stop at the bar marking the seaward edge of the 2m bench; the missing part of the profile from there to the beach is shown as a straight line. The dotted line in figure 29B is taken from a dense set of soundings made by the U.S. Coast and Geodetic

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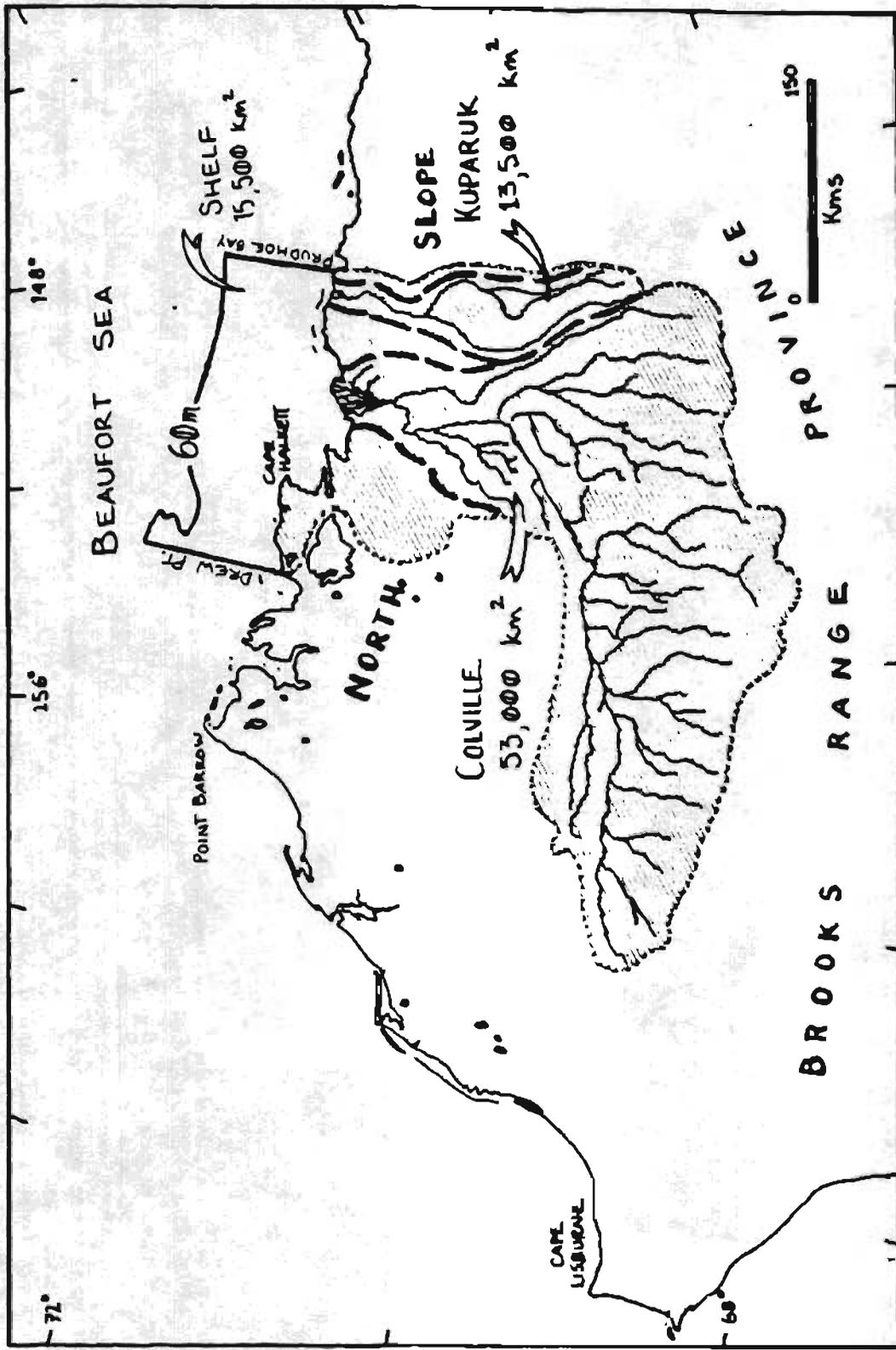


Figure 1. Map of Drainage and Shelf Areas considered in our study.

Table 1

SUMMARY OF ANNUAL SEDIMENT YIELD			
FROM COASTAL EROSION:			
Overall Erosion Rate = 2.1 m/yr			
without Colville Delta sector = 2.4 m/yr			
		Per Kilometer	Total
Bluffs	volumes =	3500m ³	1200000m ³
	weights =	8600tm	2300000tm
Offshore	volumes =	3800m ³	1300000m ³
	weights =	7200tm	2500000tm
Total	volumes =	7300m ³	2500000m ³
	weights =	13800tm	4700000tm
FROM RIVER INPUT:			
	Combined Drainage Area	74000km ²	
	Average Denudation Rate	50tm/km ²	
	volumes =	1950000m ³	
	weights =	3700000tm	

Table 2

Sample Location	Grain Size %			Reference
	gravel	sand	mud	
Oliktok Pt. & Kavearak Pt.	0	69	31	R. Lewellen 1973 writ. comm. (average of 2 smpls.)
*Simpson Lagoon	0	85	15	S. Rawlinson 1983 writ. comm. (average of 60 smpls.)
!#Tigvariak Isl.	2.6 2.5	62.9 61.9	34.5 35.6	Reimnitz & Barnes unpub. (average of 2 smpls.)
Atigaru Pt.	0	85	15	R. F. Black 1964
Drew Pt.	0	8	92	
Teshekpuk L.	0	42	58	
!Christie Pt.	0	32	68	

* organic component up to 41% of overall bluff composition

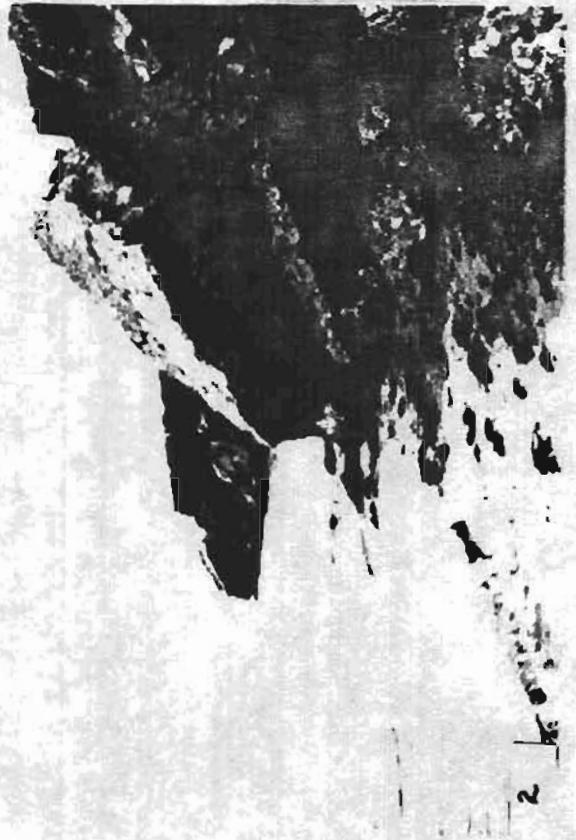
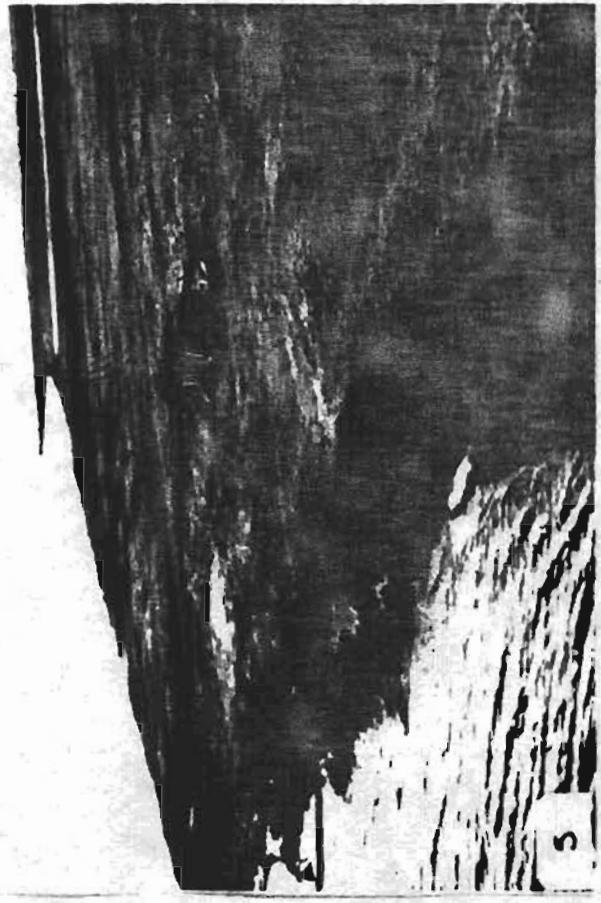
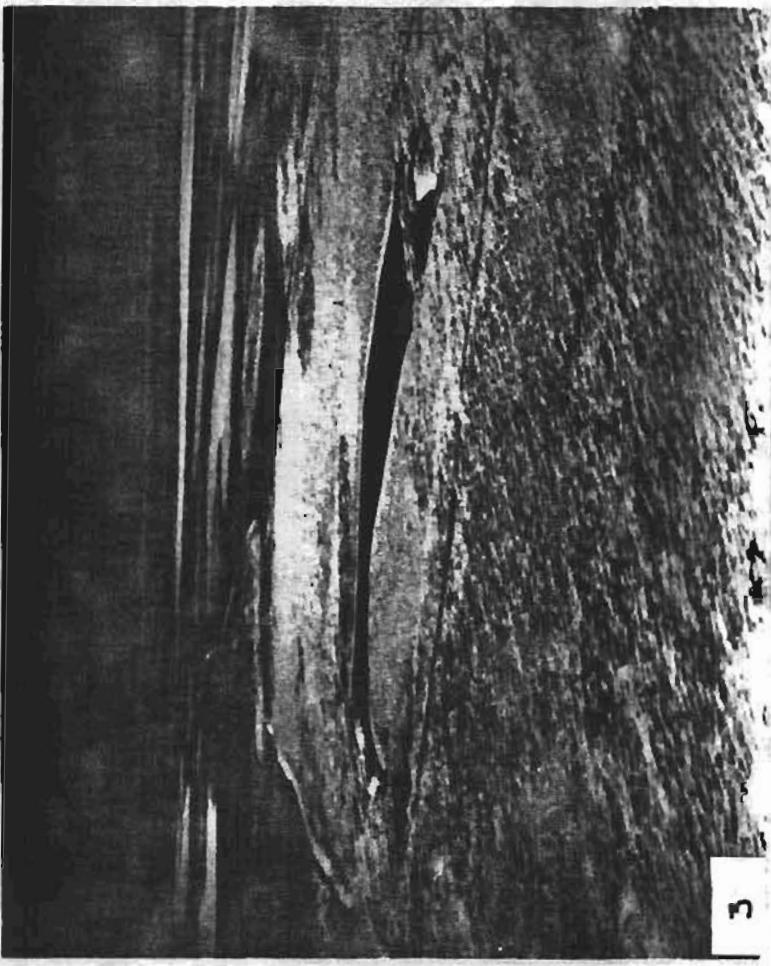
! chosen for its unusually rich accumulation of gravels

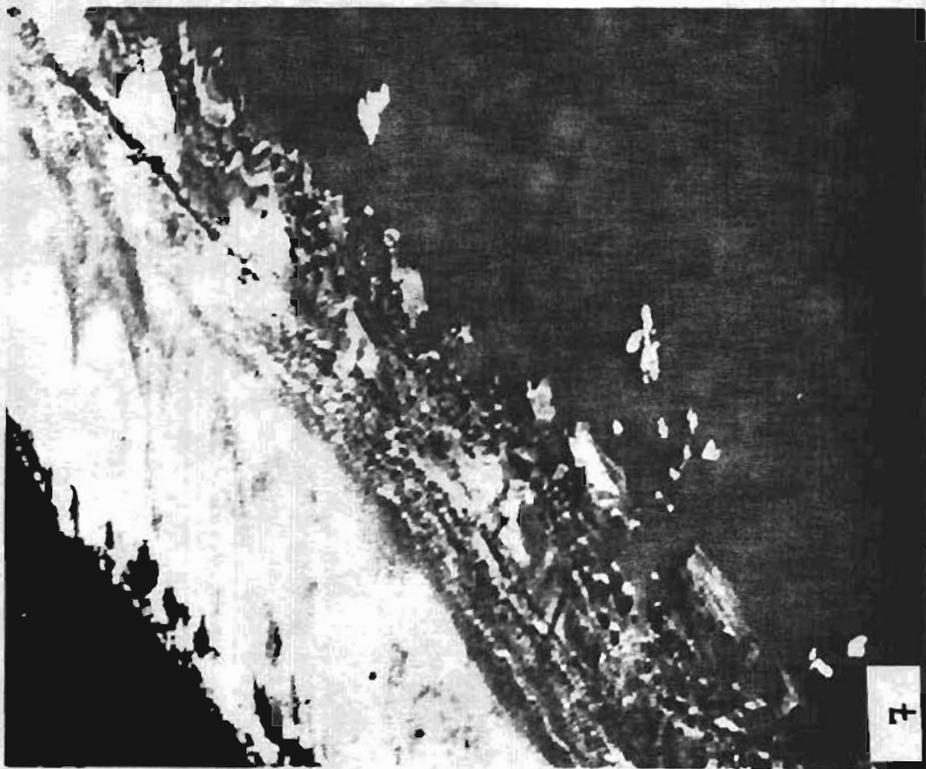
location outside of study area

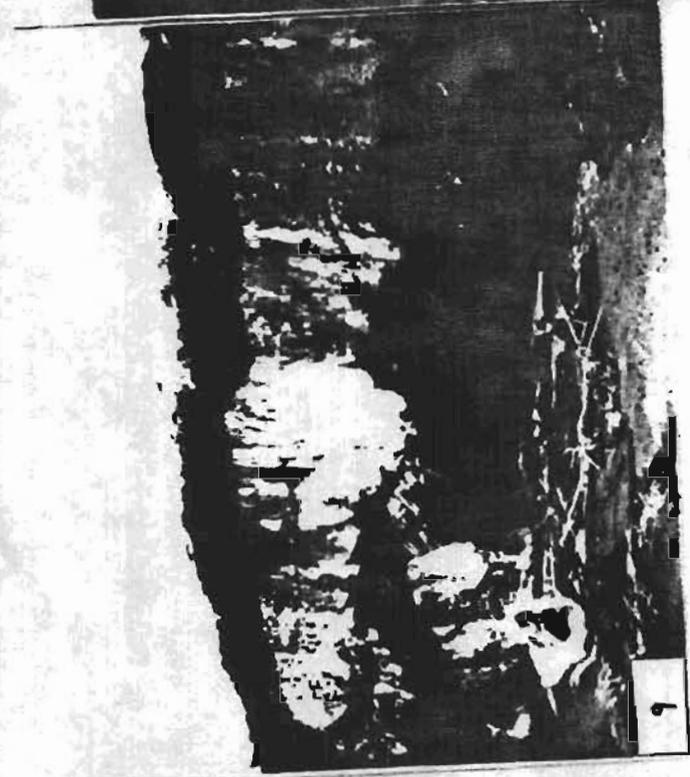
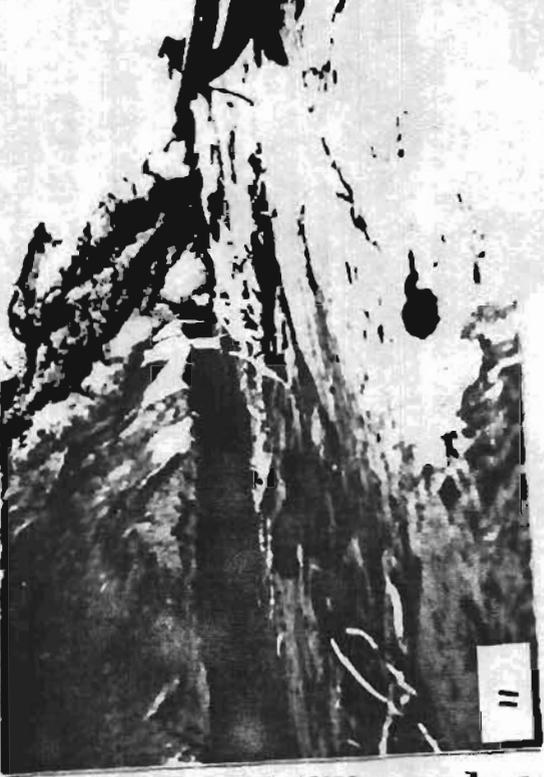
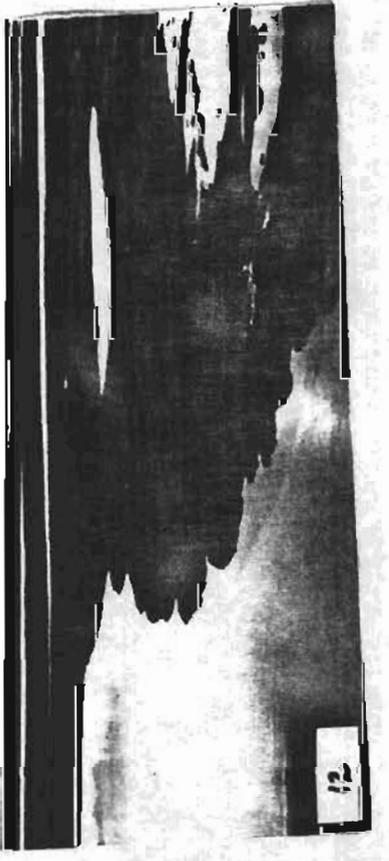
- Figure 2. Slumping of 2 m bluff following formation of basal niche.
- Figure 3. June 20 photograph of Pogik Bay and flat, lake dotted coastal plain prior to breakup of fast-ice.
- Figure 4. Aerial photographs comparing the coastline at Esook in 1949 and 1981 demonstrating 410 m of bluff retreat. The near vertical arrows point to the same hut on the two photos (from Kovacs, 1983).
- Figure 5. Low altitude oblique photo of last remaining hut at Esook Trading Post (from Kovacs, 1983).
- Figure 6. Aerial photograph of a beach transgressing over low tundra with ice wedge polygons (from Kovacs, 1983).
- Figure 7. Low altitude oblique photo of seaward side of a barrier island showing ice-wallow relief.
- Figure 8. Pillows of anchor ice (underwater ice attached to submerged objects) found widespread in shallow coastal waters during freeze-up storms. The pillow in the foreground is 50cm across and attached to medium grained unfrozen sands at 5m water depths.
- Figure 9. Fresh exposure of a 2 m high coastal bluff cutting massive ice in longitudinal section.
- Figure 10. Cross section of ice wedge in cryoturbated sandy bluff (glove for scale).
- Figure 11. Erosional niche at the base of a high bluff in aeolian (dune) sands.
- Figure 12. Erosion of low, vegetated, inactive delta front.
- Figure 13. Silt flats on prograding part of delta.
- Figure 14. Thetis Island: A) gently sloping beach in 1979 after a winter of ice-override, note striated slope B) beach scarp on september 12, 1982 C) and on october 9, 1982 after fall storm.
- Figure 15. Gravel covered ice rubble pile.
- Figure 16. A) ice wallowing in surf zone, and B) the resulting relief.
- Figure 17. Low coastal plain marked by two storm surge lines.
- Figure 18. Freshly undercut 3 m high bluff.
- Figure 19. Typical summer conditions on seaward-facing beach.

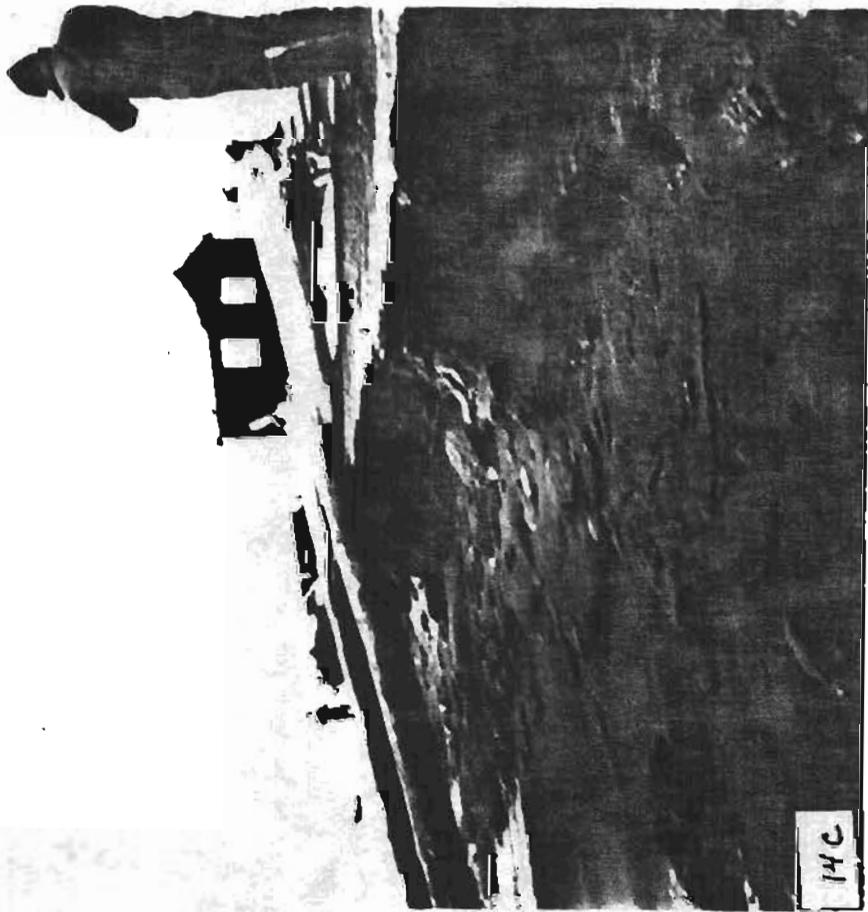
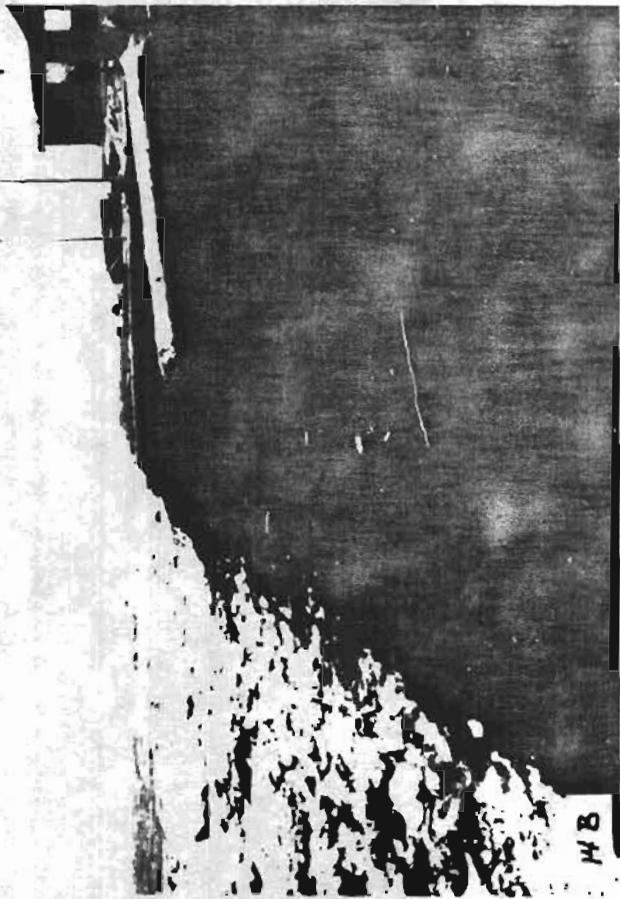
Figure 20. Landsat image (August 1, 1976) of central study area showing:

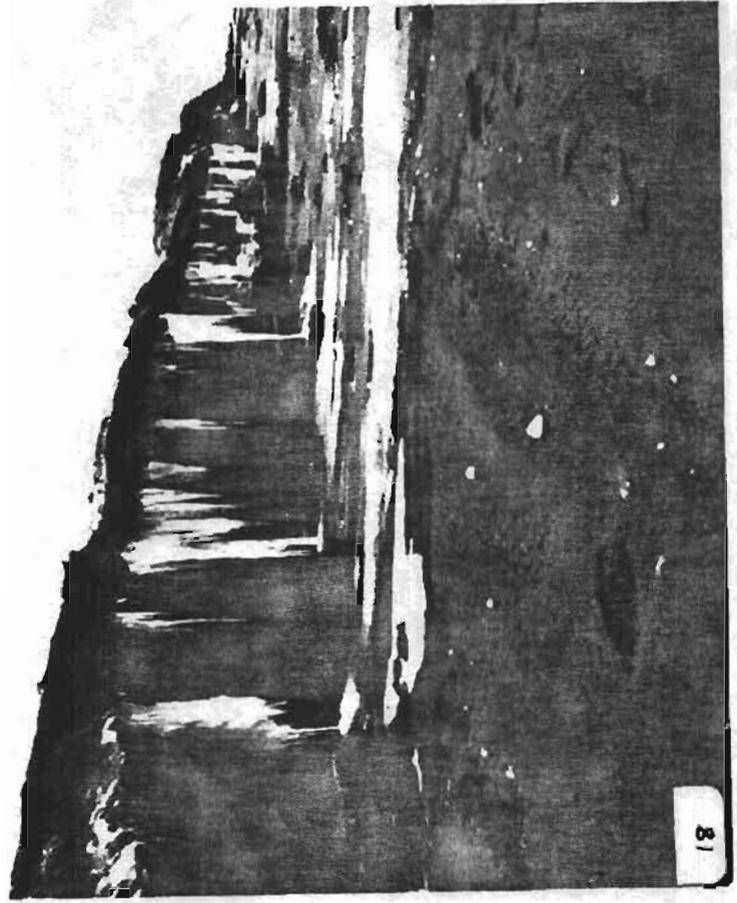
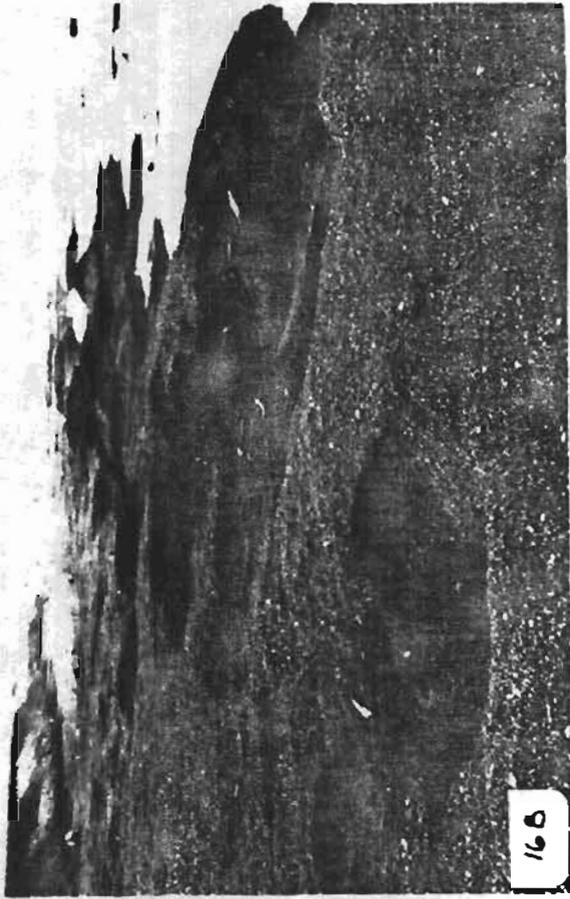
- 1) typical summer ice distribution, restricting significant fetch to warm and sheltered waters,
- 2) absence of protecting barriers along Cape Halkett coast, where most sediment is introduced,
- 3) tundra-covered older surfaces (including numerous islands), versus recent, active, and barren surfaces (delta flats and barrier islands),
- 4) deep (over 2m) ice covered lakes versus shallow ones, and
- 5) sediment-laden waters around the stagnant Colville Delta.



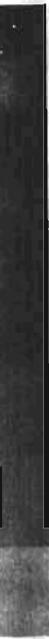
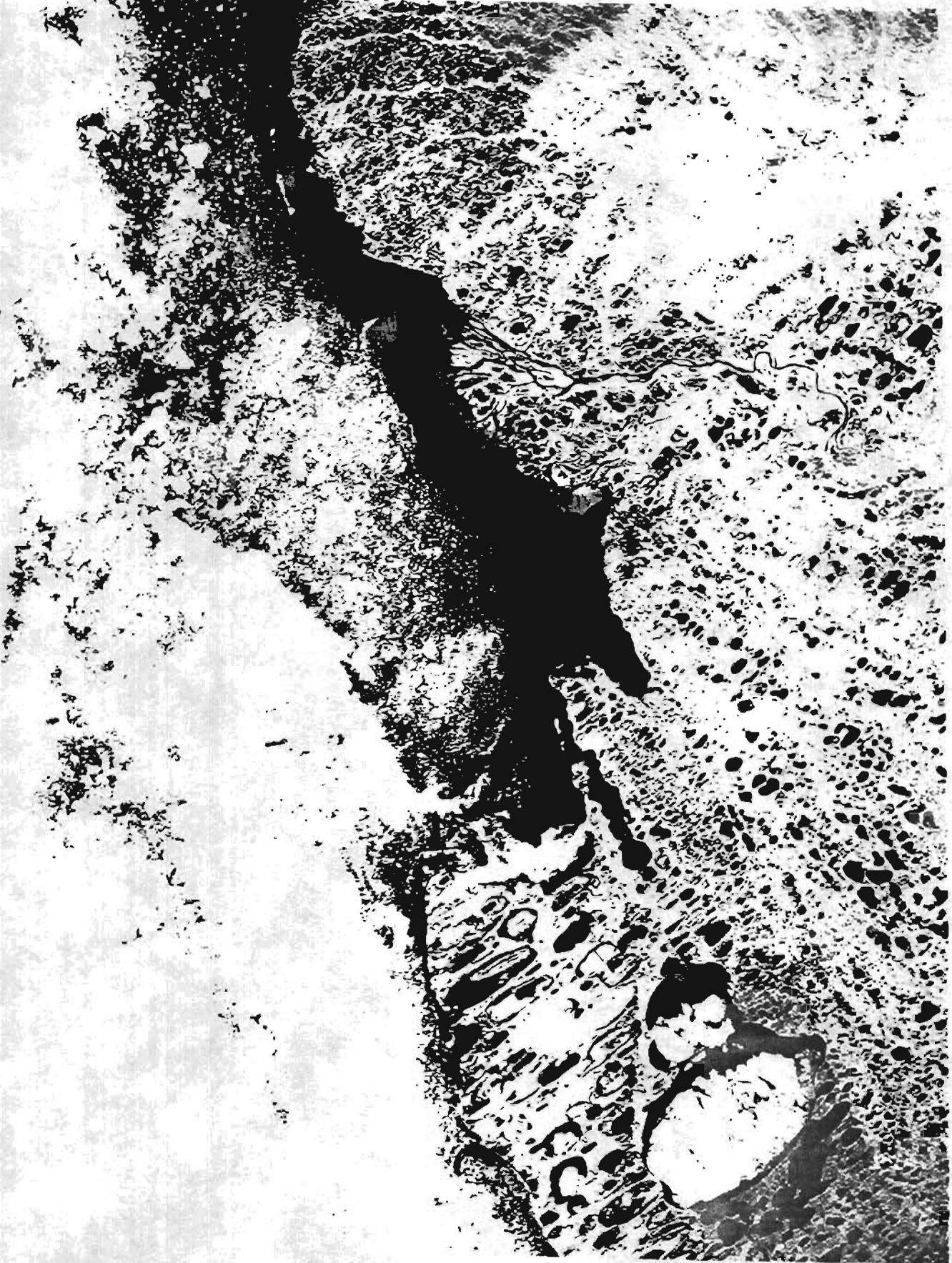












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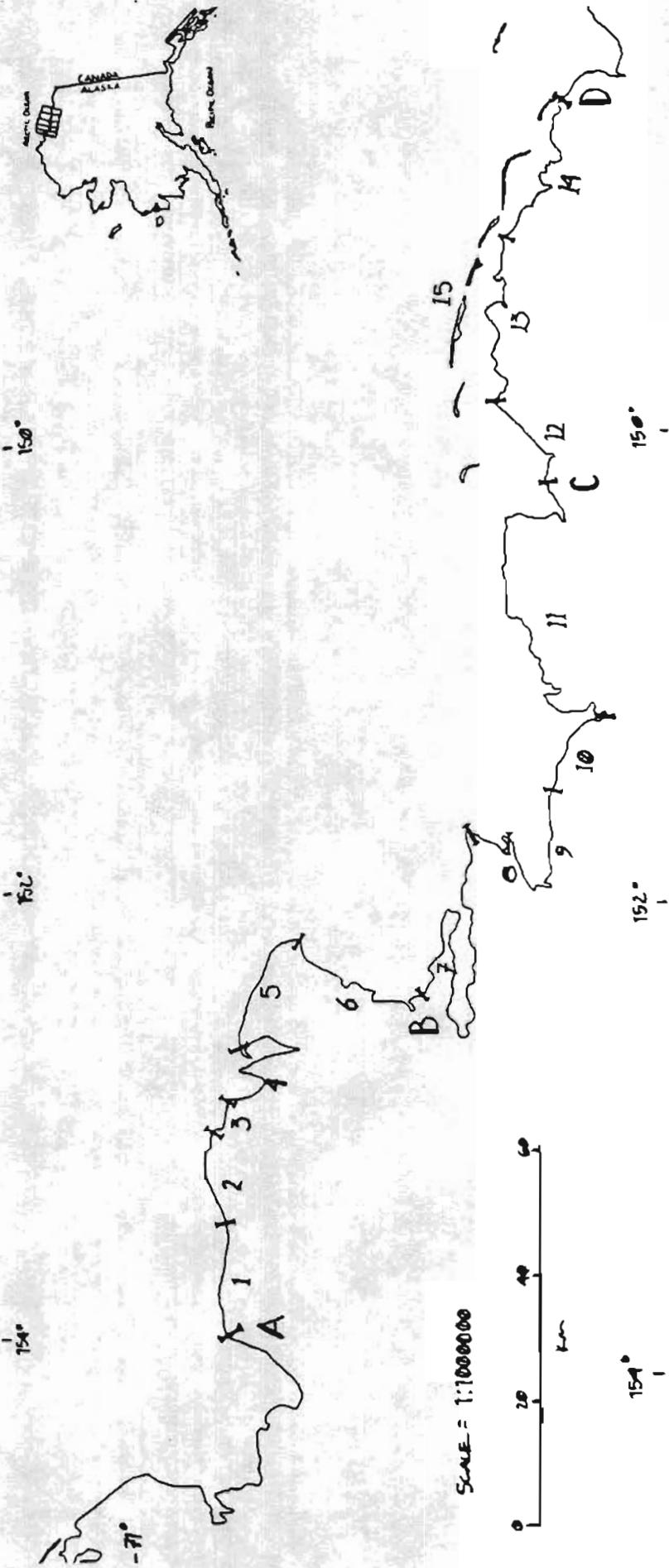
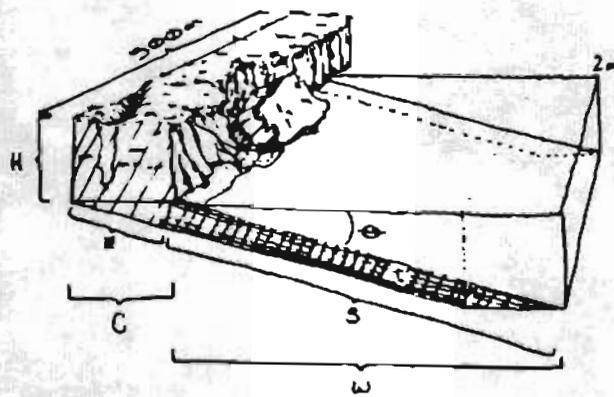


Figure 21. Index map for the 3 major coastal segments represented on this mapsheet, and for the 15 sectors for which calculations are tabulated in the appendix.



MEASURED PARAMETERS

500m segment length
 H bluff height
 C change +/- in coastline
 w distance to 2m isobath

CALCULATED PARAMETERS

θ offshore slope = $(\arctan 2/w)$
 s width of offshore polyhedron = $(2/\sin\theta)$
 t thickness of offshore polyhedron = $(C\sin\theta)$
 secondary prism width = $(C/\cos\theta)$

EQUATIONS

v_i (initial bluff volume) = $500(HC+0.5st)$
 v_1 (bluff volume - excess ice%) = $v_i - \text{excess ice}\%$
 v_2 (offshore polyhedron volume) = $500(st-0.5st)$
 V (total volume input) = $v_1 + v_2$
 T (total weight input in metric tonnes) = $1.89V$

Figure 22. General geometry used for volume calculations:

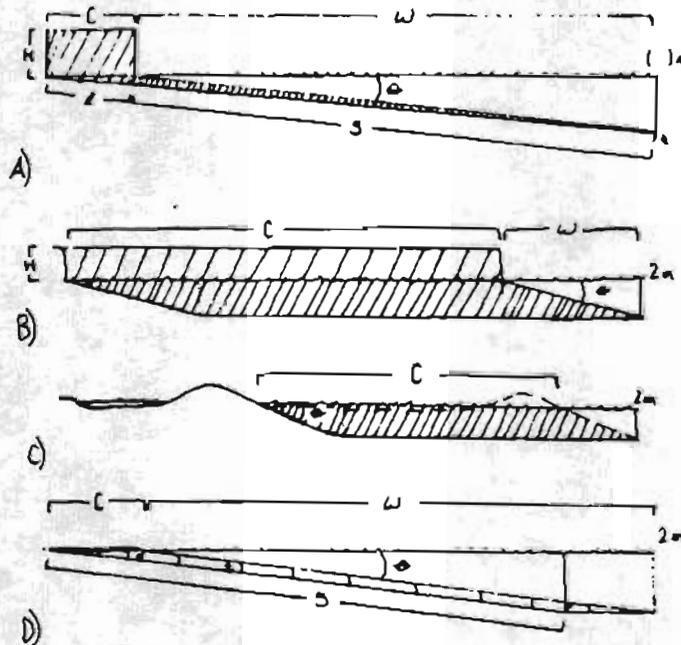


Figure 24. Special case geometries:

- A) where segment borders lagoon with a maximum depth < 2 m
 $v_i = 500(HC+0.5st)$, $v_1 = v_i - \text{excess ice}\%$, $v_2 = 0.5(500st)$
 B) where $C > W$
 $v_i = 500HC$, $v_1 = v_i - \text{excess ice}\%$, $v_2 = 500C^2$
 C) where barrier or spit shifted onshore
 $v_i = 0$, $v_1 = 0$, $v_2 = 500C^2$
 D) where accretion has occurred
 $v_i = v_1 = +500HC$, $v_2 = +500st$

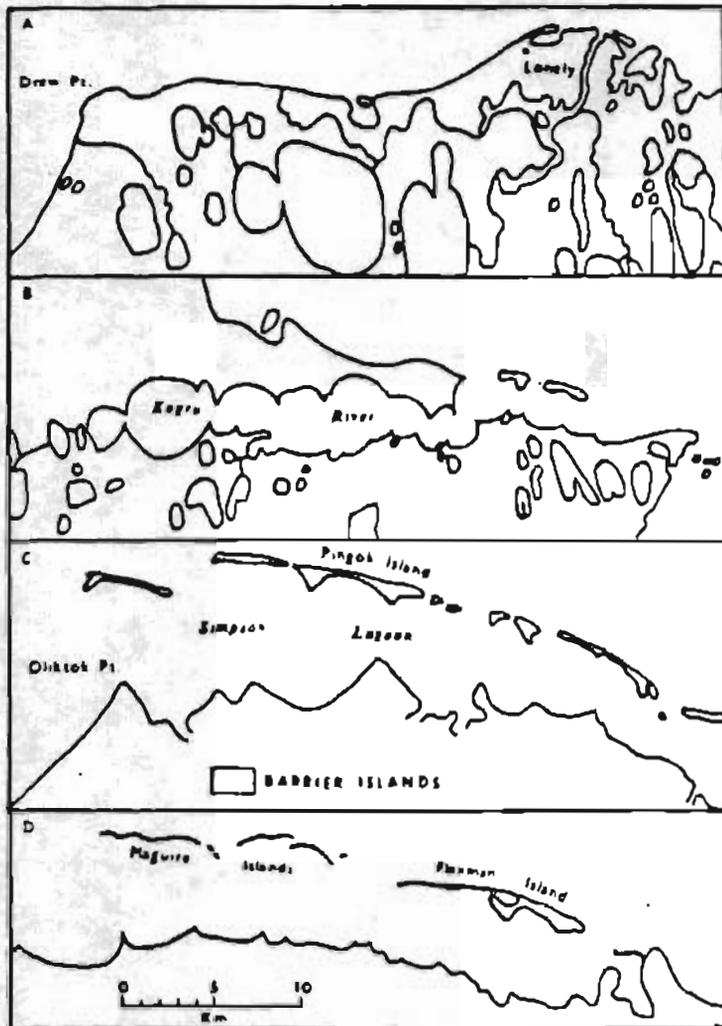


Figure 27. Sequence of lagoon formation and barrier island isolation by thaw-lake coalescence. A) initial tapping, draining, and coalescing of lakes, B) continued coalescing of lakes and thermal erosion of shoreline, C) continued thermal erosion and isolation of offshore tundra remnants, D) erosion of tundra remnants and reworking of sand and gravel into offshore barriers (from Wiseman, et al., 1973).

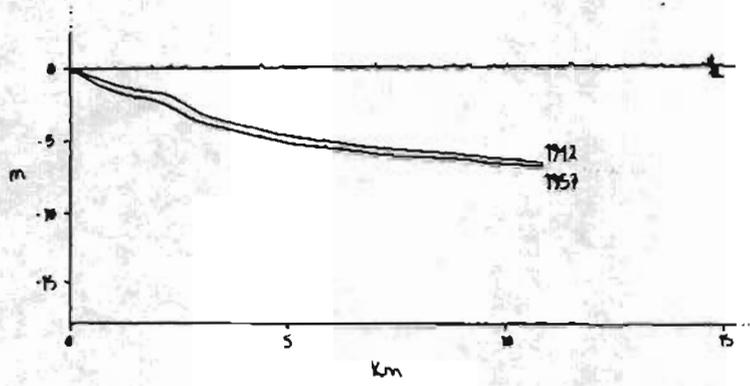


Figure 28. Comparison of hydrographic surveys repeated after 15 yrs in the East Siberian Sea (after Klyuyev 1968).

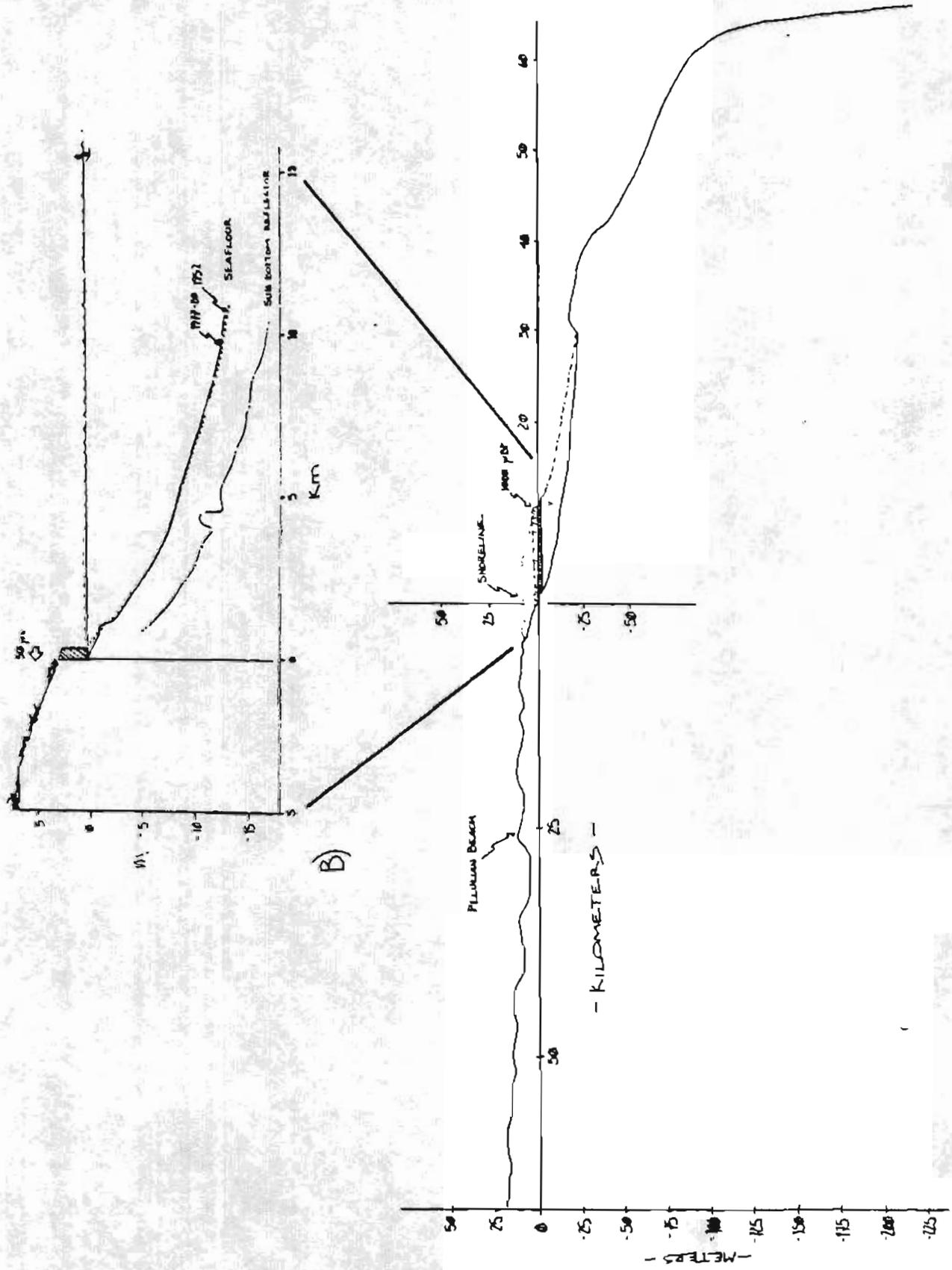
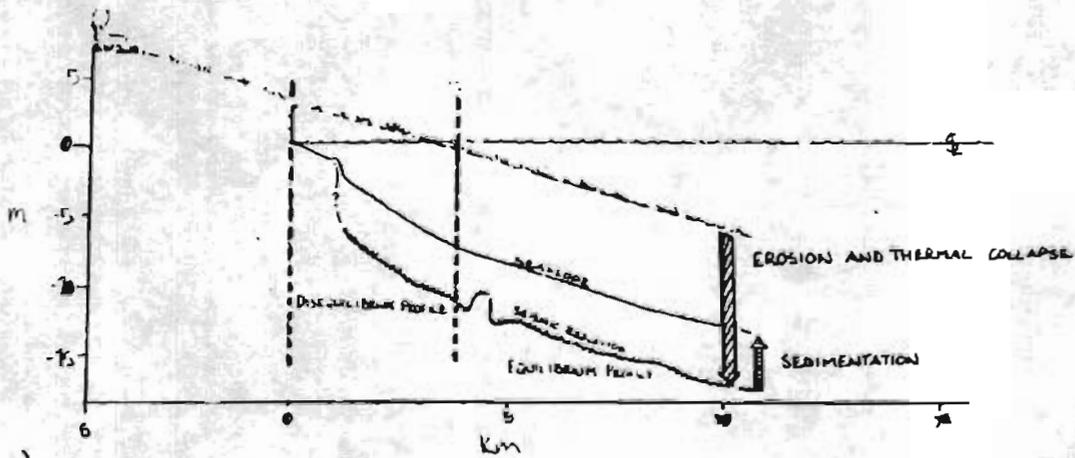
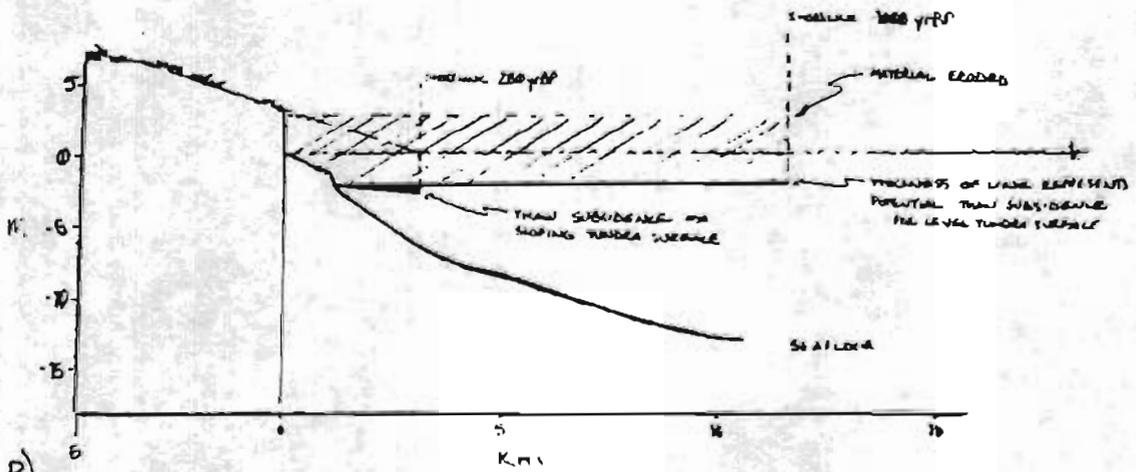


Figure 29 Coastal plain/shelf profile along line indicated on figure 26
 A) present profile and 1000 yr hindcast with accounted and unaccounted volumes indicated, B) detailed coastal profile showing a 30 year comparison of bluff and sea floor, and a shallow seismic reflector.

A)



A)



B)

Figure 26. Same profile as figure 25B with hypothetical tundra surfaces, A) possible origin of the seismic reflector as the old land surface after erosion, thaw subsidence and Holocene sedimentation, and B) potential thaw settlement below the -2m truncation surface for both level and sloping tundra surfaces assuming deep thaw.

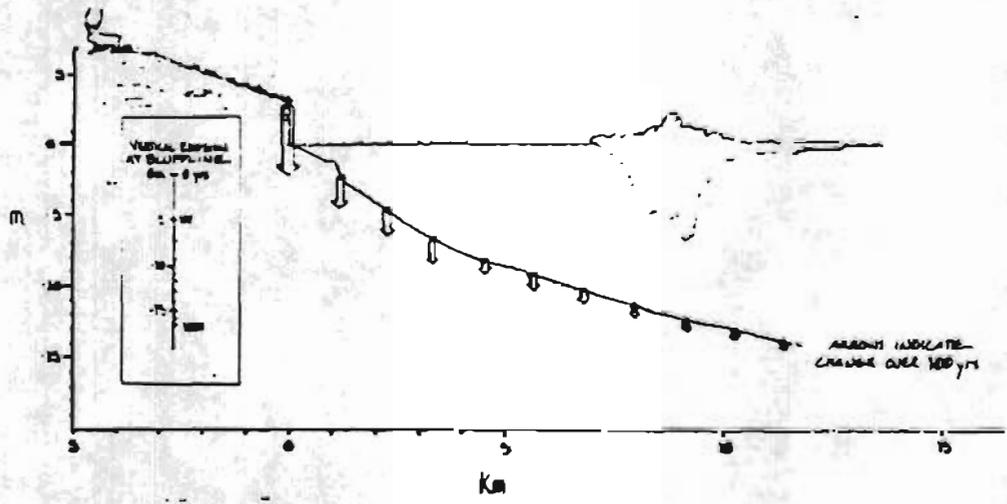


Figure 31. Present land and seafloor surface with arrows indicating vertical erosion predicted for the next hundred years at 1 km intervals along the profile; inset shows thousand year vertical erosion predicted for a point at the present shore.

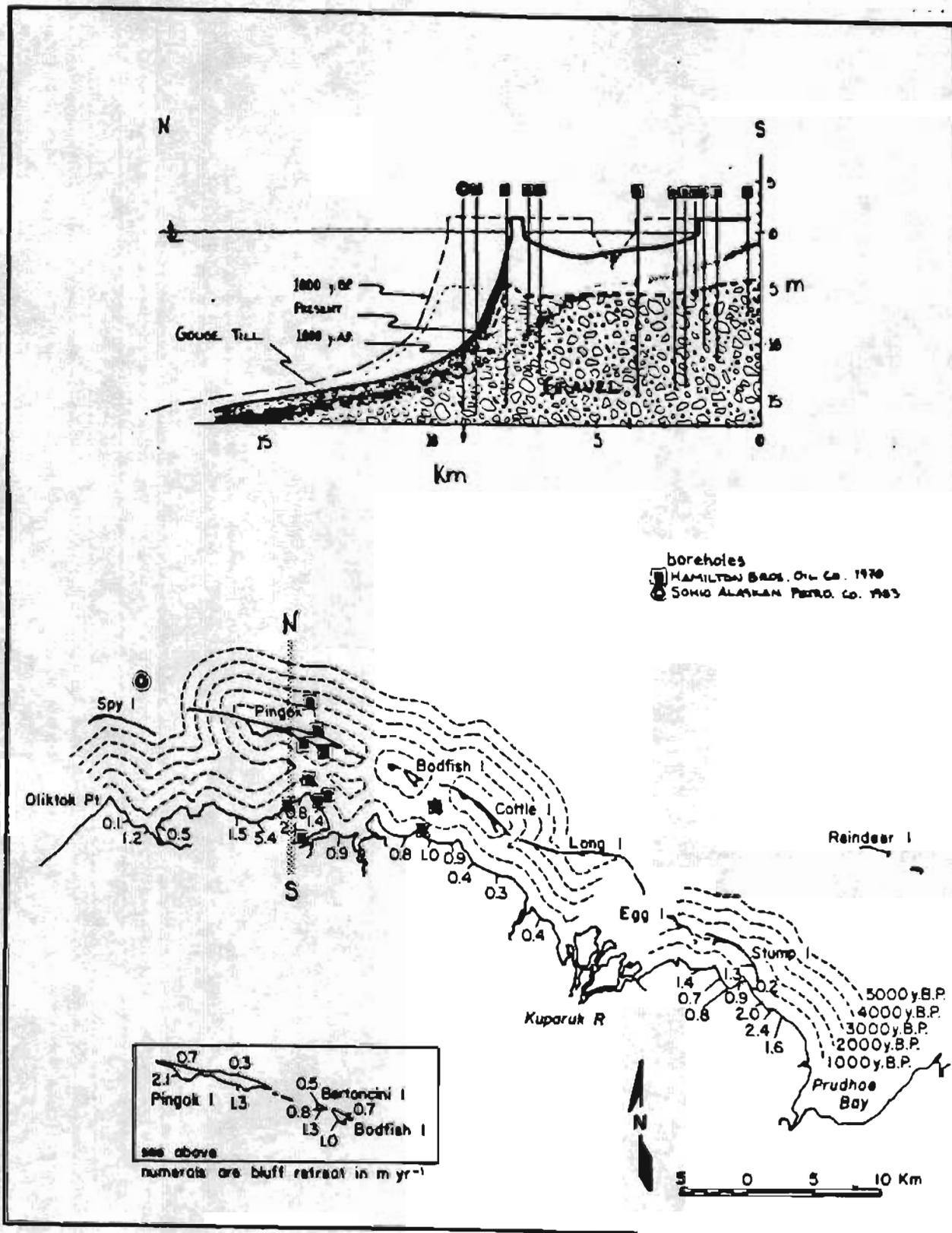


Figure 32. Simpson Lagoon paleoshorelines (after Naidu et al. 1984) and our interpretation of lagoon profile evolution. Depths to massive fluvial gravel generalized from soil borings.

APPENDIX (individual sector tabulations)

SECTOR # 1 Length: 19 km Average Retreat Rate: 8.3 m/yr

Segment No.	Onshore		Offshore					Totals		
	H	C	v1	v1	ϕ^*	w	t	y2	volume	tons
1	4.0	150	300000	246000	0.23	500	0.60	128000	374000	707000
2	4.0	230	460000	380000	0.19	600	0.77	186000	566000	1070000
3	4.0	240	480000	394000	0.14	800	0.60	204000	598000	1130000
4	4.0	230	460000	380000	0.14	800	0.57	197000	577000	1090000
5	4.0	230	460000	380000	0.13	850	0.54	199000	579000	1094000
6	4.0	220	440000	360000	0.13	850	0.52	191000	551000	1041000
7	4.0	210	420000	344000	0.14	800	0.52	182000	526000	994000
8	4.0	220	440000	360000	0.15	750	0.59	188000	548000	1036000
9	4.0	300	600000	492000	0.16	700	0.86	236000	728000	1376000
10	4.0	350	700000	574000	0.19	600	1.17	248000	822000	1554000
11	4.0	380	760000	623000	0.29	400	1.90	199000	822000	1554000
12	4.0	300	600000	492000	0.25	450	1.33	200000	692000	1308000
13	4.0	280	560000	459000	0.29	400	1.40	182000	641000	1211000
14	4.0	230	460000	377000	0.25	450	1.00	171000	548000	1036000
15	4.0	300	600000	492000	0.25	450	1.33	200000	692000	1308000
16	4.0	350	700000	574000	0.25	450	1.56	214000	788000	1489000
17	4.0	400	800000	656000	0.23	500	1.60	240000	896000	1693000
18	4.0	480	960000	787000	0.25	450	2.13	224000	1011000	1911000
19	4.0	450	900000	738000	0.33	350	2.57	161000	899000	1699000
20	4.0	350	700000	574000	0.36	320	2.19	159000	733000	1385000
21	3.5	360	630000	498000	0.33	350	2.06	175000	673000	1272000
22	3.0	330	495000	376000	0.29	400	1.65	194000	570000	1077000
23	3.0	300	450000	342000	0.25	450	1.33	200000	542000	1024000
24	2.0	280	280000	196000	0.22	510	1.10	203000	399000	754000
25	2.0	280	280000	196000	0.19	600	0.93	215000	411000	777000
26	2.0	200	200000	140000	0.18	650	0.62	169000	309000	584000
27	2.0	210	210000	147000	0.18	650	0.65	176000	323000	610000
28	2.0	200	200000	140000	0.16	700	0.57	171000	311000	588000
29	2.0	180	180000	112000	0.16	700	0.46	142000	254000	480000
30	2.0	180	180000	124000	0.19	600	0.60	153000	277000	524000
31	2.0	270	270000	189000	0.25	450	1.20	189000	378000	714000
32	2.0	270	270000	189000	0.29	400	1.30	179000	368000	696000
33	2.0	190	190000	133000	0.23	500	0.76	154000	287000	542000
34	2.0	170	170000	119000	0.19	600	0.57	146000	266000	501000
35	2.0	140	140000	98000	0.20	580	0.48	123000	221000	418000
36	2.0	120	120000	84000	0.19	600	0.40	108000	192000	363000
37	2.0	50	50000	35000	0.19	600	0.17	48000	83000	157000
38	2.0	0	0	0	0.20	580	0	0	0	0
TOTALS ($\times 10^3$) :			18095	12800				6654	19454	36767

SECTOR # 2 Length: 12.5 km Average Retreat Rate: 1.3 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v _i	v _l	ϕ^*	w	l	v ₂	volume	loss
1	1.5	0	0	0	0.23	500	0	0	0	0
2	1.5	20	15000	10000	0.29	400	0.10	19000	29000	55000
3	1.5	50	38000	25000	0.38	300	0.33	46000	71000	134000
4	1.5	100	75000	49000	0.46	250	0.80	80000	129000	244000
5	1.5	110	82000	53000	0.57	200	1.10	80000	133000	251000
6	1.5	90	68000	44000	0.55	210	0.88	71000	115000	217000
7	1.5	30	22000	14000	0.55	210	0.29	28000	42000	79000
8	1.5	30	22000	14000	0.57	170	0.35	27000	41000	77000
9	3.0	0	0	0	0.57	200	0	0	0	0
10	1.5	20	15000	10000	0.55	210	0.19	19000	29000	55000
11	0.4	60	12000	8000	0.88	130	0.92	46000	54000	102000
12	0.4	100	0	0	2.29	50	4.00	25000	25000	47000
13	0.4	80	0	0	1.64	70	2.29	24000	24000	45000
14	0.4	100	20000	13000	3.81	30	6.85	15000	28000	53000
15	1.5	60	45000	29000	3.81	30	3.99	15000	44000	83000
16	1.5	0	0	0	0.95	120	0	0	0	0
17	0.4	20	4000	3000	1.15	100	0.40	18000	21000	40000
18	0.4	120	24000	16000	3.81	30	7.98	15000	31000	59000
C 19	0.4	0	0	0	1.60	270	7.54	270000	270000	510000
C 20	0.4	0	0	0	1.60	270	7.54	270000	270000	510000
C 21	0.4	0	0	0	1.60	270	7.54	270000	270000	510000
C 22	0.4	0	0	0	1.60	270	7.54	270000	270000	510000
C 23	0.4	0	0	0	1.60	270	7.54	270000	270000	510000
24	1.5	20	15000	10000	0.35	150	0.13	19000	29000	55000
D 25	0.4	+20	0	0	0.38	320	0.06	+21000	+21000	+40000
TOTALS ($\times 10^3$) :			457	298				1876	2174	4106

SECTOR # 3 Length: 6 km Average Retreat Rate: 7.8 m/yr

Segment No.	Onshore		Offshore				Totals			
	H	C	v _i	v ₁	Q [*]	w	t	v ₂	volume	tons
1	3.0	100	150000	114000	0.11	1000	0.20	95000	209000	395000
2	1.5	300	270000	176000	0.11	1000	0.60	255000	431000	815000
3	1.5	450	422000	274000	0.09	1200	0.75	368000	640000	1210000
4	1.5	280	240000	156000	0.09	1300	0.43	250000	406000	767000
5	1.5	40	30000	20000	0.07	1500	0.06	395000	415000	784000
6	1.5	100	78000	49000	0.05	2200	0.09	98000	147000	278000
7	1.5	220	168000	108000	0.05	2200	0.02	209000	317000	599000
8	1.5	270	167000	109000	0.04	2400	0.18	200000	309000	584000
9	1.5	300	245000	159000	0.05	2200	0.27	280000	439000	830000
10	1.5	190	152000	99000	0.05	2000	0.19	181000	280000	529000
11	1.5	310	245000	159000	0.05	2200	0.28	288000	447000	845000
12	1.5	200	160000	104000	0.08	2000	0.20	190000	294000	556000
TOTALS (x10 ³) :			2323	1527				2807	4334	8192

SECTOR # 4 Length: 11 km Average Retreat Rate: Pogik Bay ~0.4 m/yr, barrier ~7.3 m/yr

Segment No.	Onshore		Offshore				Totals			
	H	C	v1	v1	°	w	t	v2	volume	tons
D 1	1.5	+70	+52000	+52000	0	0	0	0	+52000	+98000
D 2	1.5	+100	+75000	+75000	0	0	0	0	+75000	+142000
D 3	1.5	+80	+80000	+80000	0	0	0	0	+80000	+113000
D 4	1.5	+120	+90000	+90000	0	0	0	0	+90000	+170000
5	1.5	0	0	0	0	0	0	0	0	0
D 6	2.0	+80	+80000	+80000	0	0	0	0	+80000	+113000
7	2.0	0	0	0	0	0	0	0	0	0
8	2.0	0	0	0	0	0	0	0	0	0
9	2.0	20	20000	14000	0	0	0	0	14000	26000
10	1.5	70	52000	34000	0	0	0	0	34000	84000
11	1.5	100	75000	49000	0	0	0	0	49000	93000
12	1.5	130	98000	64000	0	0	0	0	64000	121000
13	1.5	120	90000	59000	0	0	0	0	59000	112000
14	1.5	120	90000	59000	0	0	0	0	59000	112000
15	1.5	130	98000	64000	0	0	0	0	64000	121000
16	1.5	170	127000	83000	0	0	0	0	83000	157000
17	1.5	200	150000	98000	0	0	0	0	98000	185000
18	1.5	200	150000	98000	0	0	0	0	98000	185000
D 19	0.2	+100	+10000	+10000	0.06	2000	0.10	+95000	+105000	+198000
D 20	0.2	+300	+30000	+30000	0.05	2200	0.26	+298000	+328000	+620000
21	0.2	0	0	0	0.05	2200	0	0	0	0
D 22	0.2	+200	+20000	+20000	0.06	2000	0.21	+201000	+221000	+418000
C Offshore input for migrating barrier at bay mouth :								1972000	1972000	3727000
TOTALS ($\times 10^3$) :			553	225				1378	1603	3030

SECTOR # 5 Length: 22.5 km Average Retreat Rate: 7.4 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v1	v1	ϕ^*	w	t	v2	volume	tons
D 1	0.2	+80	+8000	+8000	0.07	1500	0.10	+78000	+86000	+163000
2	2.0	100	100000	70000	0.08	1500	0.13	97000	167000	316000
3	2.0	70	70000	49000	0.06	2000	0.07	69000	118000	223000
4	2.0	100	100000	70000	0.05	2100	0.10	98000	168000	318000
5	2.0	250	250000	175000	0.05	2200	0.23	236000	411000	777000
6	2.0	500	500000	350000	0.07	1800	0.63	422000	772000	1459000
7	2.0	480	480000	368000	0.08	1500	0.64	403000	769000	1453000
8	3.0	300	450000	342000	0.08	1500	0.40	270000	612000	1157000
9	2.0	160	160000	122000	0.08	1400	0.23	151000	273000	516000
10	2.0	120	120000	84000	0.08	1500	0.16	115000	199000	376000
11	2.0	110	110000	77000	0.08	1500	0.15	106000	183000	346000
12	2.0	140	140000	98000	0.10	1200	0.23	132000	230000	435000
13	3.0	60	90000	68000	0.09	1300	0.09	69000	127000	240000
14	2.0	110	110000	77000	0.11	1000	0.22	104000	181000	342000
15	3.0	100	150000	114000	0.13	880	0.23	95000	209000	395000
16	2.0	180	180000	126000	0.16	700	0.51	157000	283000	535000
17	4.0	210	420000	344000	0.11	1000	0.42	188000	532000	1006000
18	2.0	340	340000	238000	0.10	1100	0.62	287000	525000	992000
19	2.0	410	410000	287000	0.11	1000	0.88	326000	613000	1159000
20	2.0	400	400000	280000	0.11	1000	0.80	320000	600000	1134000
21	2.0	280	280000	196000	0.15	980	0.57	240000	436000	824000
22	4.0	300	600000	492000	0.13	900	0.67	250000	742000	1402000
23	2.0	260	260000	182000	0.13	900	0.58	222000	404000	764000
24	2.0	250	250000	175000	0.13	900	0.56	215000	390000	737000
25	3.0	130	195000	148000	0.10	1100	0.24	122000	270000	510000
26	3.0	110	165000	125000	0.10	1100	0.20	104000	229000	433000
27	2.0	120	120000	84000	0.10	1100	0.22	113000	197000	372000
28	2.0	250	250000	175000	0.11	1000	0.50	219000	394000	745000
29	2.0	300	300000	210000	0.12	960	0.62	253000	463000	875000
30	3.0	300	450000	342000	0.12	980	0.61	254000	596000	1126000
31	3.0	300	450000	342000	0.16	990	0.80	255000	597000	1128000
32	2.0	260	260000	182000	0.12	970	0.54	225000	407000	769000
33	2.0	310	310000	217000	0.13	900	0.69	257000	474000	896000
34	2.0	400	400000	280000	0.16	720	1.11	289000	569000	1075000
35	3.0	400	600000	456000	0.19	600	1.33	267000	723000	1367000
36	2.0	300	300000	210000	0.19	600	1.00	225000	435000	822000
37	2.0	250	250000	175000	0.24	480	1.04	185000	360000	680000
38	2.0	120	120000	84000	0.23	500	0.48	106000	190000	359000
39	3.0	80	120000	91000	0.16	700	0.23	75000	166000	314000
40	3.0	70	105000	80000	0.13	900	0.16	67000	147000	278000
41	3.0	100	150000	114000	0.11	1000	0.20	95000	209000	395000
42	1.0	100	50000	30000	0.09	1300	0.15	96000	126000	238000
43	1.0	200	100000	60000	0.08	1500	0.27	187000	247000	467000
44	1.0	370	185000	111000	0.08	15000	0.50	324000	435000	822000
45	1.0	400	200000	120000	0.06	2000	0.40	360000	480000	907000
TOTALS ($\times 10^3$):			11042	8010				8562	16572	31321

SECTOR # 6 Length: 24 km Average Retreat Rate: 2.0 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v _i	v ₁	ϕ°	w	t	v ₂	volume	tons
1	2.0	100	100000	70000	0.14	800	0.25	94000	164000	310000
2	3.5	130	227000	179000	0.14	820	0.32	120000	299000	565000
3	3.5	100	175000	138000	0.11	1000	0.20	95000	233000	440000
4	3.5	100	175000	138000	0.11	1000	0.20	95000	233000	440000
5	3.5	90	168000	124000	0.11	1000	0.18	86000	210000	397000
6	3.5	100	175000	138000	0.13	900	0.22	94000	232000	438000
7	3.5	110	192000	151000	0.16	700	0.31	101000	252000	476000
8	3.5	120	210000	166000	0.16	700	0.34	110000	276000	522000
9	2.0	110	110000	77000	0.14	800	0.27	102000	179000	338000
10	2.0	130	130000	91000	0.13	850	0.31	120000	211000	399000
11	2.0	140	140000	98000	0.13	850	0.33	1128000	1226000	2317000
12	3.0	110	165000	125000	0.13	900	0.24	103000	228000	431000
13	3.0	100	150000	114000	0.12	940	0.21	95000	209000	395000
14	3.5	80	140000	111000	0.12	920	0.17	77000	188000	355000
15	3.5	50	88000	70000	0.13	910	0.11	49000	119000	225000
16	3.5	0	0	0	0.10	1100	0	0	0	0
17	3.5	20	35000	28000	0.10	1200	0.03	20000	48000	91000
18	3.5	40	70000	55000	0.09	1250	0.06	39000	94000	178000
19	3.5	30	52000	41000	0.07	1700	0.04	89000	130000	246000
20	3.5	100	175000	138000	0.07	1700	0.12	97000	235000	444000
21	2.0	100	100000	70000	0.08	1400	0.14	96000	166000	314000
22	2.0	100	100000	70000	0.07	1800	0.12	97000	167000	316000
23	1.0	150	75000	45000	0.07	1700	0.18	143000	188000	355000
24	1.0	110	55000	33000	0.09	1250	0.18	105000	138000	261000
25	2.0	100	100000	70000	0.08	1350	0.15	96000	166000	314000
26	3.0	110	165000	125000	0.09	1250	0.18	105000	230000	435000
27	3.0	110	165000	125000	0.13	900	0.24	120000	245000	463000
28	3.0	80	120000	91000	0.08	1500	0.11	78000	169000	319000
29	3.0	60	90000	68000	0.08	1500	0.08	59000	127000	240000
30	3.0	100	150000	114000	0.08	1500	0.13	97000	211000	399000
31	3.0	150	225000	171000	0.08	1500	0.20	143000	314000	593000
32	3.0	130	195000	148000	0.08	1500	0.17	124000	272000	514000
33	3.0	110	165000	125000	0.08	1500	0.15	106000	231000	437000
34	3.0	110	165000	125000	0.09	1300	0.17	105000	230000	435000
35	3.0	100	150000	114000	0.07	1600	0.12	97000	211000	399000
36	3.0	100	150000	114000	0.06	2000	0.10	98000	212000	401000
37	3.0	100	150000	114000	0.04	3000	0.07	98000	212000	401000
38	3.0	100	150000	114000	0.04	3000	0.07	98000	212000	401000
39	3.0	120	185000	140000	0.03	3300	0.07	118000	258000	488000
40	3.0	110	165000	125000	0.03	3600	0.06	108000	233000	440000
41	3.0	80	120000	91000	0.03	3500	0.05	79000	170000	321000
42	3.0	40	60000	46000	0.03	3400	0.02	40000	86000	162000
43	3.0	20	30000	23000	0.03	3400	0.01	20000	43000	81000
44	3.0	20	30000	23000	0.03	3400	0.01	20000	43000	81000
45	3.0	20	30000	23000	0.03	3400	0.01	20000	43000	81000
46	3.0	20	30000	23000	0.03	3400	0.01	20000	43000	81000
47	3.0	40	60000	46000	0.03	3400	0.02	40000	86000	163000
48	4.0	70	140000	115000	0.03	3400	0.04	69000	184000	348000
TOTALS (x10 ³) :			5987	4543				5113	9656	18250

SECTOR # 7 Length: 24.5 km Average Retreat Rate: 1.4 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v1	v1	ϕ^*	w	t	v2	volume	tons
1	3.0	90	125000	103000	0.03	4000	0.06	89000	192000	363000
2	3.0	110	165000	125000	0.03	4000	0.06	108000	233000	440000
3	3.0	100	150000	114000	0.04	3000	0.07	98000	212000	401000
4	3.0	80	90000	68000	0.04	2800	0.04	59000	127000	240000
5	3.0	0	0	0	0.04	2800	0	0	0	0
6	3.0	100	150000	114000	0.05	2500	0.08	98000	212000	401000
7	3.0	90	135000	103000	0.06	2000	0.09	88000	191000	361000
8	3.0	180	270000	205000	0.08	1400	0.26	168000	373000	705000
9	3.0	0	0	0	0.10	1200	0	0	0	0
10	3.0	140	210000	160000	0.15	750	0.37	127000	287000	543000
11	3.0	130	195000	148000	0.79	800	0.43	116000	264000	499000
12	3.0	100	150000	114000	0.23	500	0.39	90000	204000	386000
13	4.0	20	40000	33000	0.23	500	0.08	20000	53000	100000
14	4.0	20	40000	33000	0.21	550	0.07	20000	53000	100000
15	4.0	0	0	0	0.23	500	0	0	0	0
16	4.0	0	0	0	0.79	800	0	0	0	0
17	3.0	20	30000	23000	0.13	850	0.05	20000	43000	81000
18	3.0	20	30000	23000	0.12	950	0.04	20000	43000	81000
19	3.0	50	75000	57000	0.11	1050	0.10	49000	106000	200000
20	3.0	50	75000	57000	0.10	1150	0.10	49000	106000	200000
21	3.0	30	90000	68000	0.10	1150	0.10	49000	117000	221000
22	5.0	0	0	0	0.10	1100	0	0	0	0
23	5.0	0	0	0	0.10	1100	0	0	0	0
24	5.0	30	75000	57000	0.10	1150	0.05	30000	87000	164000
25	3.0	60	90000	68000	0.10	1200	0.10	59000	127000	240000
26	3.0	60	90000	68000	0.09	1250	0.10	59000	127000	240000
27	5.0	70	175000	148000	0.09	1300	0.11	68000	216000	408000
28	5.0	50	125000	108000	0.08	1350	0.15	98000	204000	386000
29	1.0	100	50000	30000	0.08	1350	0.15	96000	126000	238000
30	4.0	0	0	0	0.05	2500	0	0	0	0
31	4.0	0	0	0	0.05	2500	0	0	0	0
32	4.0	0	0	0	0.05	2500	0	0	0	0
33	4.0	0	0	0	0.05	2500	0	0	0	0
34	4.0	0	0	0	0.05	2500	0	0	0	0
35	4.0	0	0	0	0.05	2500	0	0	0	0
36	4.0	0	0	0	0.05	2500	0	0	0	0
37	4.0	0	0	0	0.05	2500	0	0	0	0
38	4.0	0	0	0	0.05	2500	0	0	0	0
39	4.0	0	0	0	0.05	2500	0	0	0	0
40	4.0	0	0	0	0.05	2500	0	0	0	0
41	4.0	0	0	0	0.05	2500	0	0	0	0
42	2.0	0	0	0	0.05	2500	0	0	0	0
43	2.0	0	0	0	0.05	2500	0	0	0	0
44	2.0	30	30000	21000	0.04	3200	0.02	30000	51000	96000
45	2.0	70	70000	49000	0.04	2600	0.05	69000	118000	223000
46	2.0	60	60000	42000	0.05	2300	0.05	59000	101000	191000
47	2.0	100	100000	70000	0.08	1900	0.10	97000	167000	316000
48	1.0	100	50000	30000	0.07	1600	0.12	97000	127000	240000
49	1.0	20	50000	30000	0.08	1450	0.03	20000	50000	95000

Input not calculated for Eskimo Islands; no significant net change.

TOTALS ($\times 10^3$) : 2295 2289 2048 4317 8159

SECTOR # 8 Length: 8.5 km Average Retreat Rate: 1.7 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v1	v1	•	w	t	v2	volume	tons
1	2.0	70	70000	49000	0.05	2400	0.06	69000	118000	223000
2	2.0	70	70000	49000	0.04	3000	0.05	69000	118000	223000
3	2.0	50	50000	35000	0.03	3500	0.03	49000	84000	169000
4	2.0	0	0	0	0.03	3300	0	0	0	0
5	2.0	0	0	0	0.03	3500	0	0	0	0
6	2.0	0	0	0	0.03	3600	0	0	0	0
7	2.0	0	0	0	0.03	3800	0	0	0	0
8	2.0	20	20000	14000	0.03	4000	0.01	20000	34000	64000
9	2.0	50	50000	35000	0.03	4000	0.03	50000	85000	161000
12	2.0	0	0	0	0.03	4000	0	0	0	0
11	2.0	0	0	0	0	0	0	0	0	0
12	2.0	0	0	0	0	0	0	0	0	0
13	2.0	0	0	0	0	0	0	0	0	0
14	2.0	0	0	0	0	0	0	0	0	0
15	2.0	0	0	0	0	0	0	0	0	0
16	2.0	0	0	0	0	0	0	0	0	0
17	2.0	30	30000	21000	0.05	2500	0.20	30000	51000	96000
18	2.0	20	20000	14000	0.05	2500	0.20	20000	34000	64000
19	2.0	0	0	0	0.05	2300	0	0	0	0

Total of Offshore spits, bars, flats :

126000 23814000

TOTALS (x10³) :

433 902 1705

SECTOR # 9 Length: 23 km Average Retreat Rate: 0.7 m/yr

Segment No.	Onshore		Offshore						Totals	
	H	C	v1	v1	\bar{v}	w	t	v2	volume	tons
1	3.0	0	0	0	0.08	1500	0	0	0	0
2	4.0	0	0	0	0.08	1500	0	0	0	0
3	3.0	0	0	0	0.08	1500	0	0	0	0
4	3.0	0	0	0	0.08	1500	0	0	0	0
5	4.0	0	0	0	0.10	1200	0	0	0	0
6	2.0	0	0	0	0.09	1300	0	0	0	0
7	3.0	0	0	0	0.10	1200	0	0	0	0
8	2.0	0	0	0	0.09	1300	0	0	0	0
9	5.0	0	0	0	0.09	1300	0	0	0	0
10	3.0	0	0	0	0.07	1800	0	0	0	0
11	2.0	20	20000	14000	0.07	1800	0.03	20000	34000	64000
12	3.0	0	0	0	0.07	1500	0	0	0	0
13	3.0	20	30000	23000	0.07	1800	0.03	20000	43000	81000
14	4.0	20	40000	33000	0.07	1700	0.02	20000	53000	100000
15	2.0	20	20000	14000	0.07	1700	0.02	20000	34000	64000
16	2.0	40	40000	28000	0.08	1500	0.05	39000	67000	127000
17	4.0	40	80000	66000	0.08	1500	0.05	39000	105000	198000
18	2.0	100	100000	70000	0.08	1500	0.13	97000	167000	316000
19	2.0	20	20000	14000	0.08	1400	0.29	20000	34000	64000
D 20	0.2	+130	+13000	+13000	0.08	1400	0.18	+129000	+142000	+268000
21	2.0	100	100000	70000	0.10	1200	0.17	96000	166000	314000
22	2.0	80	80000	56000	0.08	1500	0.11	78000	134000	253000
23	2.0	60	60000	42000	0.06	2000	0.06	59000	101000	191000
24	2.0	70	70000	49000	0.06	2000	0.07	69000	118000	223000
25	2.0	70	70000	49000	0.07	1700	0.08	69000	118000	223000
26	3.0	60	90000	68000	0.08	1400	0.09	59000	127000	240000
27	3.0	0	0	0	0.08	1500	0	0	0	0
28	3.0	20	20000	15000	0.08	1800	0.02	20000	35000	66000
29	4.0	50	100000	82000	0.06	1800	0.06	49000	131000	248000
30	3.0	110	165000	125000	0.06	1800	0.12	107000	232000	438000
31	3.0	30	45000	34000	0.06	1900	0.03	30000	64000	121000
32	3.0	40	60000	46000	0.05	2300	0.03	40000	86000	163000
33	2.0	40	40000	28000	0.05	2300	0.03	40000	68000	129000
34	2.0	20	20000	14000	0.06	2300	0.02	20000	34000	64000
35	3.0	30	45000	34000	0.06	2300	0.03	30000	64000	121000
36	4.0	20	40000	33000	0.05	2300	0.02	20000	53000	100000
37	3.0	0	0	0	0.05	2300	0	0	0	0
38	3.0	20	30000	23000	0.06	2300	0.02	20000	43000	81000
39	4.0	20	40000	33000	0.05	2300	0.02	20000	53000	100000
40	4.0	20	40000	33000	0.05	2300	0.02	20000	53000	100000
41	3.0	0	0	0	0.05	2300	0	0	0	0
42	3.0	0	0	0	0.05	2300	0	0	0	0
43	3.0	0	0	0	0.05	2300	0	0	0	0
44	4.0	0	0	0	0.06	2300	0	0	0	0
45	2.0	0	0	0	0.06	2300	0	0	0	0
46	2.0	0	0	0	0.06	2300	0	0	0	0
TOTALS ($\times 10^3$) :			1452	1083				992	2075	3922

SECTOR # 10 Length: 15.5 km Average Retreat Rate: 2.5 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v1	v1	ϕ	w	t	v2	volume	tons
1	1.5	50	38000	25000	0.01	12000	0.01	50000	75000	142000
2	1.5	30	22000	14000	0.01	11000	0.005	30000	44000	83000
3	1.5	20	15000	10000	0.01	11000	0.003	20000	30000	57000
4	1.5	20	15000	10000	0.01	11000	0.003	20000	30000	57000
5	1.5	0	0	0	0.01	11400	0	0	0	0
6	3.0	0	0	0	0.01	11400	0	0	0	0
7	1.5	20	15000	10000	0.01	11000	0.003	20000	30000	57000
8	1.5	60	45000	29000	0.01	11000	0.01	60000	89000	168000
9	1.5	100	75000	49000	0.01	10700	0.02	99000	148000	280000
10	1.5	130	98000	64000	0.01	10500	0.02	129000	193000	365000
11	1.5	90	68000	44000	0.01	10500	0.02	90000	134000	253000
12	1.5	100	75000	49000	0.01	10000	0.02	99000	148000	280000
13	1.5	90	68000	44000	0.01	10000	0.02	90000	134000	253000
14	1.5	80	60000	39000	0.01	10000	0.02	80000	119000	225000
15	1.5	90	68000	44000	0.01	10200	0.02	90000	134000	253000
16	1.5	120	90000	59000	0.01	10100	0.02	119000	178000	336000
17	1.0	20	10000	6000	0.01	10200	0.004	20000	26000	49000
18	1.0	40	20000	12000	0.01	9900	0.01	40000	52000	98000
19	1.0	60	30000	18000	0.01	10000	0.01	60000	78000	147000
20	1.0	100	50000	30000	0.01	10500	0.02	99000	129000	244000
21	1.0	140	70000	42000	0.01	10700	0.03	139000	181000	342000
22	1.0	200	100000	60000	0.01	10700	0.04	198000	258000	488000
23	1.0	100	50000	30000	0.01	11200	0.02	99000	129000	244000
24	1.0	90	45000	27000	0.01	11600	0.02	90000	117000	221000
25	1.0	90	45000	27000	0.01	12000	0.02	90000	117000	221000
26	1.0	80	40000	24000	0.01	12200	0.01	80000	104000	197000
27	1.0	90	45000	27000	0.01	12600	0.01	90000	117000	221000
28	1.0	60	30000	18000	0.01	13000	0.01	60000	78000	147000
29	1.5	70	53000	34000	0.01	13400	0.01	70000	104000	196000
30	1.5	100	75000	49000	0.01	13700	0.01	100000	149000	282000
31	1.5	50	38000	25000	0.01	13800	0.01	50000	75000	142000
TOTALS ($\times 10^3$) :			1453	919				2281	3200	6048

SECTOR # 11 Length: 48 km Average Retreat Rate: +.4 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v _i	v _l	σ^*	w	t	v ₂	volume	tons
1	0.5	40	10000	6000	0.01	14000	0.006	40000	46000	87000
2	0.5	20	5000	3000	0.01	13600	0.003	20000	23000	43000
3	0.5	40	10000	6000	0	0	0	0	6000	11000
4	0.5	30	7000	4000	0	0	0	0	4000	8000
5	0.5	20	5000	3000	0	0	0	0	3000	6000
6	0.5	50	12000	7000	0	0	0	0	7000	13000
7	0.5	50	12000	7000	0	0	0	0	7000	13000
8	0.5	20	5000	3000	0	0	0	0	3000	6000
D 9	0.2	+60	+6000	+6000	0	0	0	0	+6000	+11000
10	0.5	0	0	0	0.1	3500	0	0	0	0
11	0.5	100	25000	14000	0.01	12400	0.10	70000	84000	159000
12	0.5	80	20000	11000	0	0	0	0	11000	21000
13	0.5	20	5000	3000	0	0	0	0	3000	6000
14	0.5	0	0	0	0.01	11000	0	0	0	0
15	0.5	30	7000	4000	0.01	10450	0.01	50000	54000	102000
16	0.5	80	20000	11000	0	0	0	0	11000	21000
17	0.4	100	20000	20000	0.01	9700	0.02	99000	119000	226000
18	0.4	70	14000	14000	0.01	8900	0.02	70000	84000	159000
19	0.4	90	18000	18000	0.01	8600	0.02	90000	108000	204000
20	0.4	110	22000	22000	0.01	8000	0.03	110000	132000	249000
21	0.4	230	46000	46000	0.02	7400	0.06	226000	272000	514000
22	0.4	180	32000	32000	0.02	7200	0.04	158000	190000	359000
D 23	0.2	+110	+11000	+11000	0.02	7200	0.03	+109000	+120000	+227000
24	0.4	140	28000	28000	0.02	7200	0.04	139000	167000	316000
D 25	0.2	+220	+22000	+22000	0.02	7100	0.06	+217000	+239000	+452000
26	0.5	0	0	0	0.01	8200	0	0	0	0
D 27	0.2	+150	+15000	+15000	0.01	8700	0.03	+149000	+164000	+310000
D 28	0.2	+110	+11000	+11000	0.01	8600	0.02	+109000	+120000	+227000
D 29	0.2	+20	+2000	+2000	0.01	8500	0.004	+20000	+22000	+42000
30	0.5	200	50000	29000	0.01	8100	0.04	197000	228000	427000
31	0.5	300	75000	43000	0.01	7900	0.07	294000	337000	637000
32	0.5	0	0	0	0.01	8300	0	0	0	0
33	0.5	210	52000	30000	0.01	9480	0.04	208000	238000	450000
34	0.5	200	50000	29000	0.01	10000	0.04	198000	227000	429000
35	1.0	0	0	0	0.01	10000	0	0	0	0
36	1.0	80	40000	24000	0.01	9500	0.02	80000	104000	197000
37	1.0	20	20000	12000	0.01	9650	0.004	20000	22000	44000
D 38	0.2	+100	+10000	+10000	0.01	10100	0.02	+99000	+109000	+208000
D 39	1.0	70	70000	42000	0.01	10300	0.01	70000	112000	212000
40	1.0	100	100000	60000	0.01	9800	0.02	99000	159000	301000
41	1.0	110	110000	68000	0.01	9300	0.02	109000	175000	331000
D 42	0.2	+20	+2000	+2000	0.01	9200	0.004	+20000	+22000	+42000
43	1.0	40	40000	24000	0.01	9100	0.01	40000	64000	121000
44	1.0	30	30000	18000	0.01	9000	0.006	30000	48000	91000
45	1.0	40	40000	24000	0.01	8900	0.01	40000	64000	121000
46	1.0	0	0	0	0.01	9300	0	0	0	0
47	1.0	100	100000	60000	0.01	9750	0.02	10000	70000	132000
48	1.0	200	200000	120000	0.01	10000	0.04	198000	318000	601000
49	1.0	100	100000	60000	0.01	10100	0.02	99000	159000	301000
50	0.5	110	28000	16000	0.01	10150	0.02	11000	27000	51000
51	0.5	120	30000	17000	0.01	10200	0.02	119000	136000	257000
52	0.5	120	30000	17000	0.01	10300	0.02	119000	136000	257000
53	0.5	100	25000	14000	0.01	10000	0.02	99000	113000	214000
54	0.5	120	30000	17000	0.01	9700	0.02	119000	136000	257000
D 55	0.2	+30	+3000	+3000	0.01	9400	0.006	+30000	+33000	+62000
D 56	0.2	+220	+22000	+22000	0.01	8800	0.05	+217000	+239000	+452000
57	0.2	90	9000	9000	0.01	8300	0.02	90000	99000	187000
58	0.2	320	32000	32000	0.01	7700	0.08	313000	346000	652000
59	0.2	280	28000	28000	0.02	7250	0.08	274000	302000	571000
60	0.2	160	16000	16000	0.02	7200	0.04	160000	176000	333000

(sector 11 continued)

61	0.2	200	20000	20000	0.02	7200	0.05	197000	217000	410000
62	0.2	0	0	0	0.02	7200	0	0	0	0
63	0.2	0	0	0	0.01	7700	0	0	0	0
64	0.2	0	0	0	0.01	7850	0	0	0	0
D 65	0.2	+300	+30000	+30000	0.01	7900	0.08	+290000	+320000	+605000
D 66	0.2	+410	+41000	+41000	0.01	7700	0.10	+399000	+440000	+832000
D 67	0.2	+400	+40000	+40000	0.01	7400	0.11	+389000	+429000	+811000
68	0.2	0	0	0	0.01	7600	0	0	0	0
69	0.2	0	0	0	0.01	7400	0	0	0	0
70	0.2	100	10000	10000	0.02	7100	0.02	99000	109000	206000
71	0.2	200	20000	20000	0.02	6950	0.05	197000	217000	410000
72	0.2	200	20000	20000	0.02	6900	0.06	197000	217000	410000
73	0.2	210	21000	20000	0.02	6700	0.06	207000	227000	429000
74	0.2	160	16000	16000	0.02	6250	0.05	158000	174000	329000
D 75	0.2	+80	+6000	+6000	0.02	5700	0.02	+60000	+66000	+125000
D 76	0.2	+500	+50000	+50000	0.02	5400	0.18	+177000	+527000	+996000
D 77	0.2	+500	+60000	+60000	0.02	5320	0.22	+566000	+626000	+1183000
D 78	0.2	+400	+40000	+40000	0.02	5400	0.15	+385000	+425000	+803000
D 79	0.2	+220	+22000	+22000	0.02	5500	0.08	+216000	+238000	+450000
D 80	0.2	+300	+30000	+30000	0.02	5300	0.11	+291000	+321000	+607000
D 81	0.2	+300	+30000	+30000	0.02	5100	0.12	+291000	+321000	+607000
D 82	0.2	+350	+35000	+35000	0.02	5000	0.14	+338000	+373000	+705000
D 83	0.2	+300	+30000	+30000	0.02	5400	0.11	+292000	+322000	+609000
D 84	0.2	+200	+20000	+20000	0.02	5100	0.08	+196000	+216000	+408000
85	0.2	0	0	0	0.02	8700	0	0	0	0
86	0.2	20	2000	2000	0.02	6550	0.005	20000	22000	42000
D 87	0.2	+200	+20000	+20000	0.01	8500	0.02	+80000	+100000	+189000
D 88	0.2	+100	+10000	+10000	0	0	0	0	+10000	+19000
89	0.2	100	10000	10000	0	0	0	0	10000	19000
90	0.2	120	12000	12000	0	0	0	0	12000	23000
91	0.2	80	8000	8000	0	0	0	0	8000	15000
92	0.2	80	8000	8000	0	0	0	0	8000	11000
93	0.2	100	10000	10000	0	0	0	0	10000	19000
94	0.2	90	9000	9000	0	0	0	0	9000	17000

D Total of Offshore spits, bars, flats :

+68000 +680000 +1285000

TOTALS ($\times 10^3$) :

824 864

+777

+113

+214

SECTOR # 12 Length: 16.5 km Average Retreat Rate: 1.6 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v _i	v _l	ϕ^*	w	t	v ₂	volume	tons
1	1.0	40	20000	12000	0.02	6000	0.01	40000	52000	98000
2	1.0	40	20000	12000	0.02	6000	0.01	40000	52000	98000
3	1.0	20	10000	6000	0.02	5500	0.01	20000	26000	49000
4	1.0	60	30000	18000	0.02	5500	0.02	60000	78000	147000
5	1.0	30	15000	9000	0.02	4500	0.01	30000	39000	74000
6	1.0	20	10000	6000	0.02	4700	0.01	20000	26000	49000
7	1.0	20	10000	6000	0.02	4700	0.01	20000	26000	49000
8	1.0	80	41000	25000	0.03	3500	0.05	79000	104000	197000
9	1.0	80	42000	25000	0.01	1300	0.12	78000	103000	195000
10	1.0	70	37000	22000	0.11	1100	0.13	68000	90000	170000
11	1.5	100	90000	50000	0.15	750	0.29	102000	161000	304000
12	1.5	100	82000	53000	0.16	700	0.29	93000	146000	276000
13	1.5	100	83000	54000	0.19	600	0.33	92000	146000	276000
14	2.0	100	110000	77000	0.23	600	0.40	92000	169000	319000
15	2.0	110	111000	78000	0.23	600	0.44	98000	176000	333000
16	2.0	80	84000	57000	0.14	800	0.20	78000	133000	251000
17	2.0	80	80000	56000	0.10	1100	0.14	77000	133000	261000
18	2.5	40	50000	37000	0.17	650	0.12	39000	76000	144000
19	2.0	70	70000	49000	0.19	600	0.23	66000	115000	217000
20	2.0	30	30000	21000	0.19	600	0.10	29000	50000	95000
21	2.25	20	22000	16000	0.16	700	0.06	20000	36000	68000
22	2.25	20	22000	16000	0.19	600	0.07	20000	36000	68000
23	1.0	0	0	0	0.19	600	0	0	0	0
24	1.25	0	0	0	0.19	600	0	0	0	0
25	2.0	0	0	0	0.19	600	0	0	0	0
26	2.0	0	0	0	0.19	600	0	0	0	0
27	1.0	0	0	0	0.23	500	0	0	0	0
28	2.0	20	20000	14000	0.19	600	0.07	20000	34000	64000
29	2.0	20	20000	14000	0.19	600	0.02	20000	34000	64000
30	1.0	20	10000	6000	0.16	700	0.02	20000	26000	49000
31	1.0	20	10000	6000	0.16	700	0.02	20000	26000	49000
32	1.0	110	65000	39000	0.16	700	0.11	101000	140000	265000
33	1.0	100	50000	30000	0.19	600	0.33	92000	122000	231000
TOTALS ($\times 10^3$) :			1244	823				1532	2355	4450

SECTOR # 13 Length: 32 km Average Retreat Rate : 1.2 m/yr

Segment No.	Onshore			Offshore				Totals		
	H	C	v1	v1	ϕ^*	w	t	v2	volume	tons
1	1.0	20	10000	8000	0.38	300	0.13	19000	25000	47000
2	2.0	20	20000	14000	0.18	700	0.08	20000	34000	64000
3	1.5	40	30000	20000	0.13	900	0.09	39000	59000	111000
4	1.5	60	38000	25000	0.11	1000	0.10	49000	74000	140000
5	1.5	0	0	0	0.07	1600	0	0	0	0
6	1.75	20	17000	11000	0.07	1700	0.02	20000	31000	59000
7	2.0	0	0	0	0.07	1700	0	0	0	0
D 8	0.2	+100	+10000	+10000	0.05	2300	0.09	+103000	+113000	+214000
D 9	0.2	+20	+2000	+2000	0.06	2000	0.02	+19000	+21000	+40000
10	1.75	0	0	0	0.07	1600	0	0	0	0
D 11	0.2	+120	+12000	+12000	0.08	1400	0.17	+122000	+134000	+253000
12	1.0	100	50000	30000	0.08	1400	0.14	96000	128000	238000
13	0.75	100	38000	22000	0.10	1200	0.17	96000	118000	223000
14	0.75	60	22000	13000	0.08	1500	0.08	59000	72000	136000
D 15	0.2	+40	+4000	+4000	0.37	3100	0.26	+40000	+44000	+83000
16	0.75	0	0	0	0.03	3300	0	0	0	0
17	0.75	0	0	0	0.03	3100	0	0	0	0
18	1.0	80	40000	24000	0.04	2900	0.06	79000	103000	195000
19	1.0	100	50000	30000	0.04	2700	0.07	98000	128000	242000
D 20	0.2	+20	+2000	+2000	0.04	260	0.01	+14000	+16000	+30000
21	1.0	20	10000	6000	0.04	2800	0.01	20000	26000	49000
22	1.0	30	15000	9000	0.04	3000	0.02	30000	39000	74000
23	1.5	70	52000	34000	0.04	3200	0.04	69000	103000	195000
24	1.0	80	40000	24000	0.03	3300	0.05	79000	103000	195000
25	2.0	30	30000	20000	0.03	3500	0.02	30000	50000	94000
26	1.0	80	40000	24000	0.03	3700	0.04	79000	103000	195000
D 27	0.4	+20	+4000	+4000	0.03	3700	0.01	+19000	+23000	+43000
28	0.75	0	0	0	0.03	3500	0	0	0	0
D 29	0.4	+20	+4000	+4000	0.03	3400	0.01	+19000	+23000	+43000
D 30	0.4	+20	+4000	+4000	0.03	3300	0.01	+19000	+23000	+43000
31	1.5	60	45000	29000	0.04	3200	0.04	59000	88000	166000
32	1.5	80	60000	39000	0.04	2800	0.06	79000	118000	223000
33	1.0	70	35000	21000	0.06	2000	0.07	69000	90000	170000
34	1.75	40	35000	21000	0.08	1400	0.06	39000	60000	113000
35	1.75	20	12000	8000	0.11	1000	0.04	20000	28000	53000
D 36	0.4	+40	+8000	+8000	0.09	1300	0.06	+38000	+46000	+87000
37	1.75	30	26000	18000	0.06	1800	0.03	30000	48000	91000
38	1.0	0	0	0	0.03	2300	0	0	0	0
39	1.0	20	10000	8000	0.04	2700	0.01	20000	26000	49000
40	1.5	20	15000	9000	0.04	3000	0.01	20000	29000	55000
41	1.0	20	10000	8000	0.03	3500	0.01	20000	28000	49000
42	1.5	80	22000	14000	0.03	3300	0.02	30000	44000	83000
43	1.0	90	45000	27000	0.03	3400	0.05	89000	116000	219000
44	1.75	100	75000	51000	0.04	3000	0.07	98000	149000	282000
45	1.75	120	90000	51000	0.03	3500	0.07	118000	179000	338000
46	1.5	110	82000	53000	0.03	3500	0.06	108000	161000	304000
D 47	0.4	+20	+4000	+4000	0.03	3300	0.01	+19000	+23000	+43000
48	1.5	0	0	0	0.03	3300	0	0	0	0
49	2.0	100	110000	77000	0.05	2200	0.10	107000	184000	348000
50	1.0	90	45000	27000	0.10	1100	0.16	86000	113000	214000
D 51	0.4	+30	+6000	+6000	0.06	1900	0.03	+29000	+35000	+66000
52	1.25	40	25000	16000	0.05	2200	0.04	40000	56000	106000
53	1.75	90	79000	53000	0.05	2300	0.08	88000	141000	266000
54	1.25	90	56000	35000	0.05	2300	0.08	88000	123000	232000
55	1.25	90	56000	35000	0.05	2300	0.08	88000	123000	232000

(sector13 continued)

56	1.25	100	62000	39000	0.06	2000	0.10	98000	137000	259000
57	1.25	120	75000	47000	0.09	1300	0.18	114000	161000	304000
58	1.25	100	62000	39000	0.10	1100	0.18	95000	134000	253000
59	1.5	0	0	0	0.08	1800	0	0	0	0
60	1.5	20	15000	10000	0.05	2200	0.02	20000	30000	57000
61	1.0	30	15000	9000	0.05	2100	0.03	30000	39000	74000
62	1.5	40	30000	20000	0.06	1900	0.04	39000	59000	111000
63	1.5	20	15000	9000	0.08	1500	0.03	20000	29000	55000
64	1.75	70	61000	41000	0.19	600	0.23	66000	107000	202000
TOTALS (x10 ³) :			1710	1072				2219	3291	6220

SECTOR # 14 Length: 28 km Average Retreat Rate : 1.7 m/yr

Segment No.	Onshore				Offshore				Totals	
	H	C	v1	v1	σ^*	w	t	v2	volume	tons
1	1.75	20	17000	11000	0.08	1400	0.03	20000	31000	59000
2	1.75	0	0	0	0.08	1500	0	0	0	0
3	1.5	0	0	0	0.08	1800	0	0	0	0
4	1.25	20	12000	8000	0.06	1900	0.02	20000	28000	53000
5	1.75	30	26000	18000	0.07	1700	0.04	30000	48000	91000
6	2.25	0	0	0	0.07	1600	0	0	0	0
7	2.25	20	22000	16000	0.06	1800	0.02	20000	36000	68000
8	1.75	30	26000	18000	0.06	1800	0.03	30000	48000	91000
9	1.75	0	0	0	0.07	1700	0	0	0	0
10	1.75	20	17000	11000	0.06	1800	0.02	20000	31000	59000
11	1.5	0	0	0	0.08	1900	0	0	0	0
12	1.25	0	0	0	0.05	2200	0	0	0	0
13	1.25	20	12000	8000	0.04	2700	0.01	20000	28000	53000
D 14	0.4	+30	+5000	+5000	0.03	3300	0.02	+38000	+44000	+83000
D 15	0.4	+40	+8000	+8000	0.03	3500	0.02	+38000	+46000	+87000
16	2.25	20	22000	16000	0.03	4000	0.01	20000	36000	68000
17	2.25	20	22000	16000	0.02	4100	0.01	20000	36000	68000
18	1.25	60	37000	23000	0.03	3700	0.03	50000	82000	155000
19	1.25	40	25000	16000	0.03	4300	0.02	40000	56000	106000
20	2.25	0	0	0	0.02	5000	0	0	0	0
21	1.25	0	0	0	0.02	6400	0	0	0	0
22	0.75	0	0	0	0.02	6000	0	0	0	0
23	0.75	20	7000	4000	0.02	4600	0.01	20000	24000	45000
24	0.75	20	7000	4000	0.03	4500	0.01	20000	24000	46000
25	0.75	100	38000	22000	0.03	4200	0.05	99000	121000	229000
26	0.75	200	75000	44000	0.03	3700	0.11	194000	238000	450000
27	0.75	220	83000	49000	0.03	3400	0.13	213000	262000	495000
28	0.75	70	26000	15000	0.03	4000	0.04	89000	84000	159000
29	0.75	40	15000	9000	0.03	3600	0.02	40000	49000	93000
30	0.75	0	0	0	0.04	3000	0	0	0	0
31	0.75	70	26000	15000	0.04	3000	0.05	89000	84000	159000
32	0.75	100	38000	22000	0.04	3200	0.06	98000	120000	227000
A 33	0.75	50	19000	11000	0.03	3000	0.03	39000	60000	94000
A 34	0.75	200	75000	44000	0.02	3100	0.07	147000	191000	361000
A 35	0.75	210	79000	48000	0.03	2700	0.11	152000	198000	374000
A 36	0.75	180	68000	40000	0.03	2300	0.10	11000	51000	96000
A 37	0.75	0	0	0	0.03	2600	0	0	0	0
A 38	1.25	30	26000	16000	0.03	2600	0.01	11000	27000	51000
A 39	1.75	0	0	0	0.03	2500	0	0	0	0
A 40	1.75	20	17000	11000	0.03	2000	0.01	11000	22000	41000
A 41	1.75	0	0	0	0.04	1700	0	0	0	0
A 42	1.25	0	0	0	0.04	1500	0	0	0	0
A 43	0.75	0	0	0	0.05	1400	0	0	0	0
A 44	1.5	40	30000	20000	0.05	1300	0.03	20000	40000	76000
A 45	1.25	0	0	0	0.04	1700	0	0	0	0
A 46	1.75	0	0	0	0.03	2000	0	0	0	0
A 47	1.75	20	17000	11000	0.03	1700	0.01	9000	20000	38000
A 48	0.75	20	7000	4000	0.04	1400	0.01	7000	11000	21000
A 49	1.0	20	10000	6000	0.04	1300	0.01	7000	13000	24000
A 50	1.25	0	0	0	0.04	1500	0	0	0	0
A 51	1.25	0	0	0	0.03	1900	0	0	0	0
A 52	1.25	0	0	0	0.03	2000	0	0	0	0
A 53	1.25	0	0	0	0.03	1900	0	0	0	0
A 54	1.0	20	10000	6000	0.05	1200	0.02	11000	17000	32000
A 55	1.25	0	0	0	0.07	800	0	0	0	0
A 56	1.25	0	0	0	0.14	400	0	0	0	-0
TOTALS ($\times 10^3$) :			897	546				1470	2016	3811

SECTOR # 15 Length: 36.5 km Average Retreat Rate : 1.0 m/yr

Pingok Island : segments measured clockwise around island from west end.

Segment No.	Onshore				Offshore				Totals	
	H	C	vi	v1	w	t	v2	volume	tons	
1	2.25	0	0	0	0.57	200	0	0	0	0
D 2	0.4	+20	+10000	+10000	0.67	170	0.59	+43000	+53000	+100000
D 3	0.4	+30	+6000	+8000	3.81	30	2.00	+15000	+21000	+40000
4	1.25	0	0	0	1.64	70	0	0	0	0
D 5	0.4	+130	+26000	+26000	2.29	50	5.19	+130000	+156000	+295000
D 6	0.4	+120	+24000	+24000	2.29	50	4.79	+120000	+144000	+272000
7	0.75	0	0	0	1.43	80	0	0	0	0
D 8	0.4	+20	+4000	+4000	1.43	80	0.50	+20000	+24000	+45000
D 9	0.4	+30	+6000	+6000	1.43	80	0.75	+30000	+36000	+68000
D 10	0.4	+40	+8000	+8000	1.04	110	0.73	+40000	+48000	+91000
11	1.75	40	35000	24000	1.43	80	1.00	30000	54000	102000
12	1.75	20	18000	12000	1.15	100	0.40	18000	30000	57000
13	1.75	80	70000	47000	0.95	120	1.33	53000	100000	189000
B 14	0.5	100	25000	14000	2.29	50	2.00	100000	114000	215000
15	0.5	100	25000	14000	0.10	1200	0.17	96000	110000	208000
16	1.75	100	88000	59000	0.10	1200	0.17	96000	155000	293000
17	1.75	100	88000	59000	0.13	900	0.22	94000	153000	289000
18	1.75	110	96000	65000	0.23	500	0.44	98000	163000	308000
19	1.75	100	88000	59000	0.18	700	0.29	93000	152000	287000
20	1.75	100	88000	59000	0.15	750	0.27	93000	152000	287000
21	1.75	100	88000	59000	0.14	800	0.25	94000	153000	289000
22	1.75	100	70000	47000	0.11	1000	0.20	95000	142000	268000
23	2.0	80	70000	49000	0.08	1400	0.11	78000	127000	240000
24	1.75	90	79000	53000	0.07	1750	0.10	88000	141000	266000
25	1.75	60	52000	35000	0.06	1950	0.06	59000	94000	178000
26	1.25	80	50000	31000	0.06	1950	0.08	78000	109000	206000
27	1.25	80	50000	31000	0.06	1900	0.08	78000	109000	206000
28	1.25	100	63000	39000	0.07	1850	0.12	97000	136000	257000
29	2.25	80	90000	64000	0.06	1850	0.09	78000	142000	268000
30	2.25	100	112000	80000	0.06	1800	0.11	97000	177000	335000
31	2.25	30	34000	24000	0.05	2500	0.02	30000	54000	102000
Offshore input (from removal) of bar :								17000	17000	32000

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(sector 15 continued)

Bertoncini and Bodfish Islands : segments measured clockwise from west end.

Segment No.	Onshore				Offshore				Totals	
	H	C	vi	v1	w	t	v2	volume	tons	
B 1	1.75	120	105000	71000	0.95	40	2.00	120000	191000	361000
B 2	1.75	100	88000	59000	1.14	50	2.00	100000	159000	301000
B 3	2.25	120	135000	97000	0.95	40	2.00	120000	217000	410000
B 4	2.25	100	112000	80000	1.14	90	2.00	100000	180000	340000
B 5	1.75	70	61000	41000	0.57	200	0.70	58000	99000	187000
D 6	0.4	+50	+10000	+10000	0.14	775	0.12	+19000	+59000	+112000
D 7	1.75	40	0	0	2.86	0	0	0	0	0
D 8	0.4	+20	+4000	+4000	0.14	800	0.05	+20000	+24000	+46000
D 9	0.4	+20	+4000	+4000	0.13	900	0.04	+18000	+22000	+42000
D 10	0.4	+60	+12000	+12000	0.09	1300	0.01	+8000	+18000	+34000
D 11	0.4	+20	+4000	+4000	0.06	1800	0.02	+19000	+23000	+43000
D 12	0.4	+110	+22000	+22000	0.07	1700	0.13	+106000	+128000	+242000
D 13	2.25	0	0	0	0.09	1200	0	0	0	0

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